

ENERGY HARVESTING APPLICATIONS

(ICT-ENERGY SUMMER SCHOOL 2016)

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Outline for Short Course

- Introduction and Linear Energy Harvesting
- Energy Harvesting Transducers
 - Electromagnetic
 - Piezoelectric
 - Electrostatic
- Wideband and Nonlinear Energy Harvesting
- **Applications**

Outline for This Lecture

- Industrial
- Light Switches (Smart Buildings)
- Tire Pressure Monitoring
- Wearable Electronics

Some Other Application Spaces

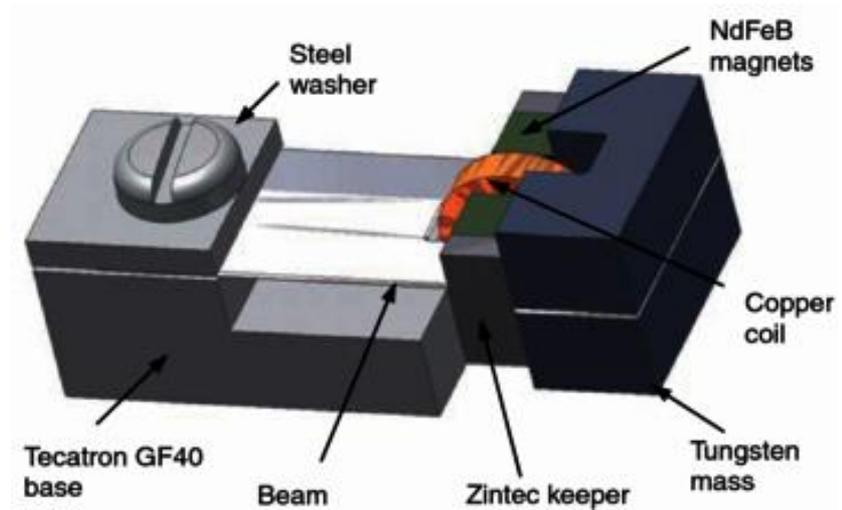
- Transportation
 - Rail cars and undercarriages
- Automotive
 - Harsh environment sensors
- Power generating pavement
 - PaveGen (www.pavegen.com)
- Asset tracking
 - Cold storage for food transport etc.
- Aerospace (sensors on/in planes and helicopters)
- Structural health monitoring sensors
 - Bridges, highways, etc.

INDUSTRIAL

Industrial Vibration Energy Harvesting

- Process control sensors in industrial environments need reliable long life power supplies
- Much of the machinery vibrates at 50 or 60 Hz
- Very low level (10's of mG) vibrations, but very consistent and stable frequency
 - Standard linear oscillator based harvesters work well
- Industries
 - Oil and gas
 - Chemical manufacturing
 - Waste water treatment
- Vibration Energy Harvesting works well and has been in use for several years

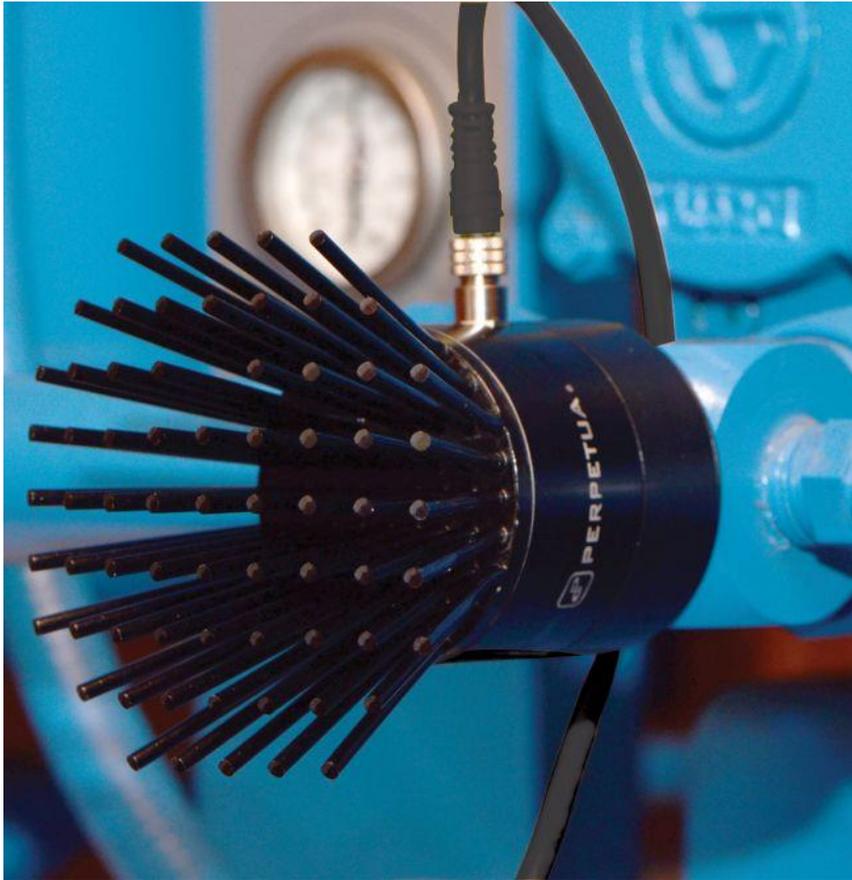
Perpetuum



<http://www.perpetuum.com/>

Beeby et. al, JMM, 2007

Perpetua Power (Thermoelectric)



<http://www.perpetapower.com/>

LIGHT SWITCHES

Why Light Switches?

- It is expensive to wire light switches for new and retrofitted buildings
- Wireless light switches can be moved based on users' convenience without rewiring
- Changing batteries in light switches in large buildings with many many switches is a significant maintenance cost and headache
- Light switches can integrate into smart building control schemes

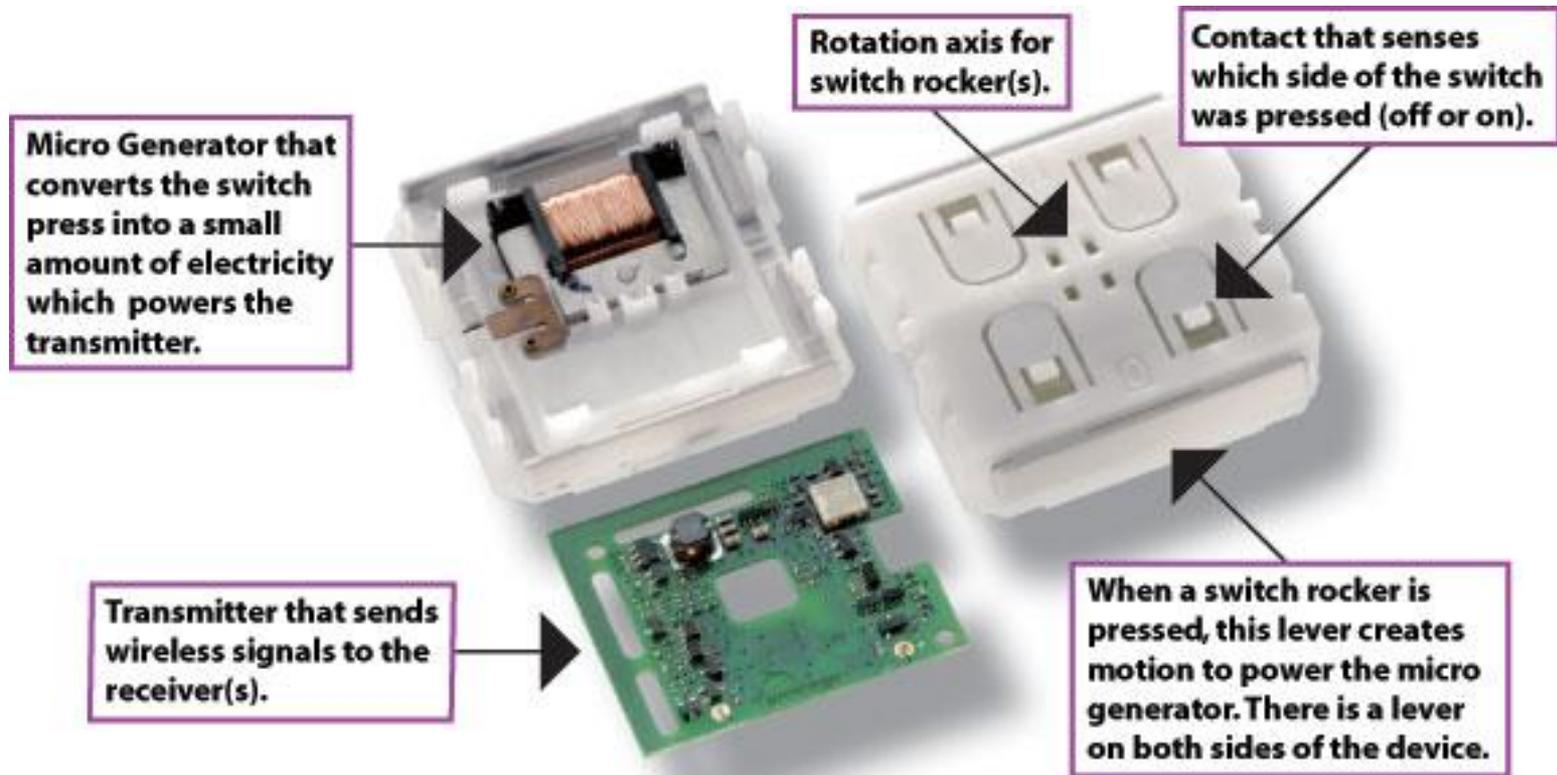
EnOcean Light Switches



EnOcean, www.enocean.com

- Fixed amount of energy input, very roughly $4 \text{ N} \times 1 \text{ mm} = 4 \text{ mJ}$ max.
- Use EnOcean's radio and communications protocol
- Needs somewhere around 100 uJ for a transmission, or 2.5% efficiency
- I believe efficiency is closer to 10%
- Note, early designs were piezoelectric

Enocean Light Switches



<http://www.adhocelectronics.com/Products/Wireless-Lighting-Control>

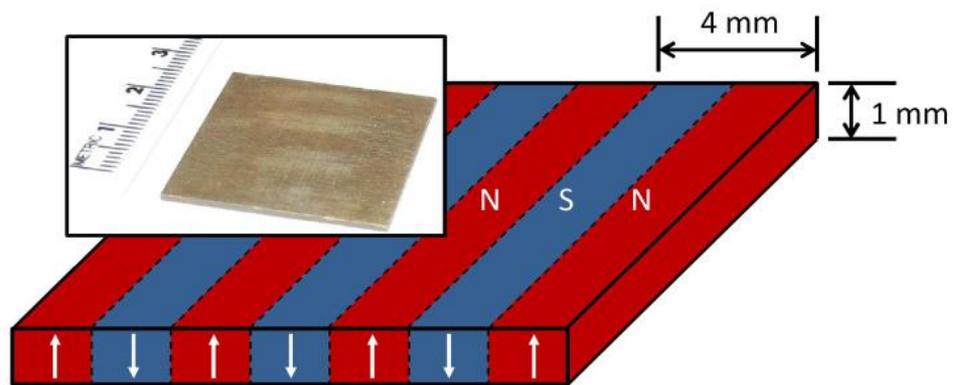
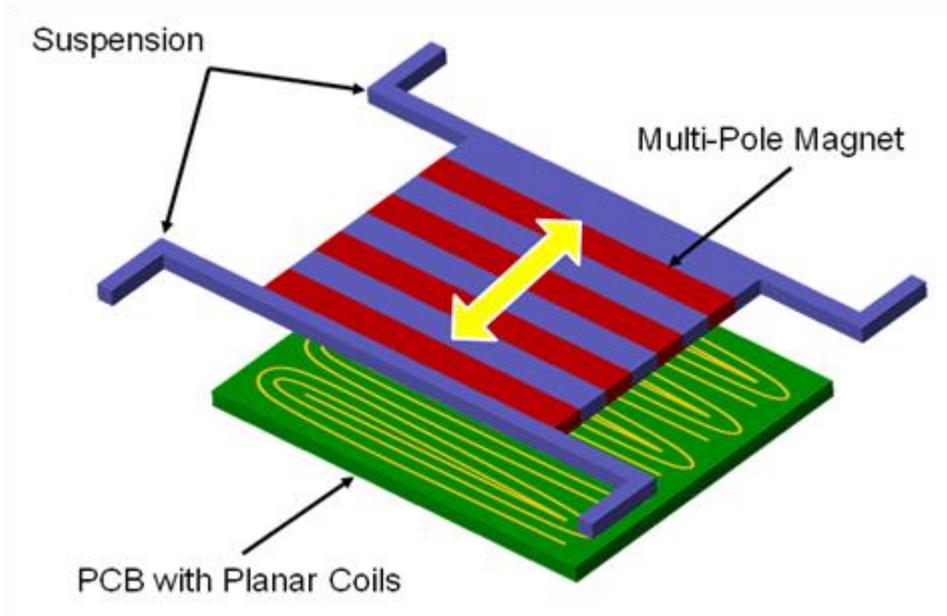
Rotational Switch

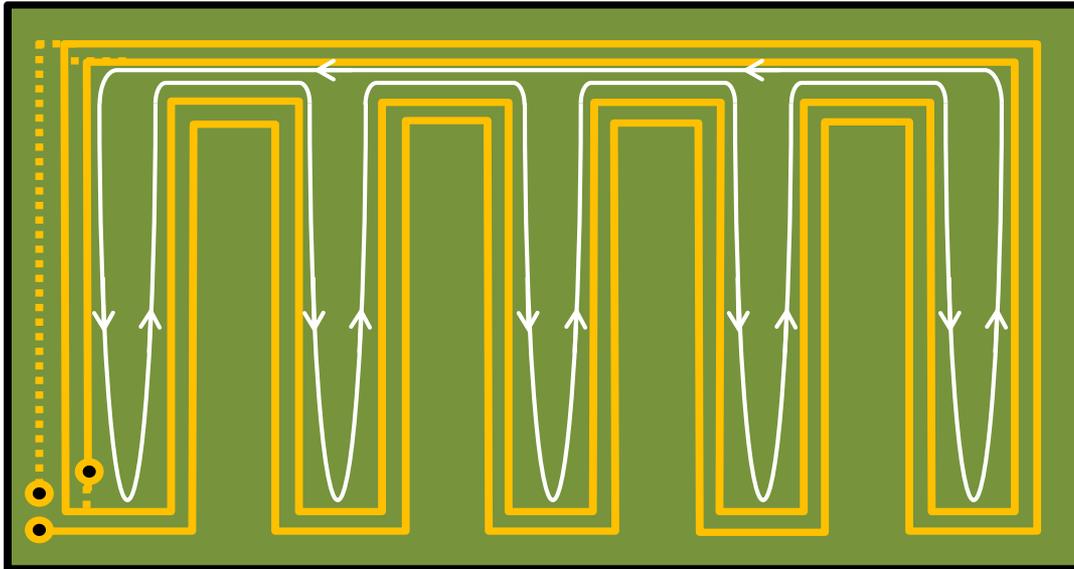
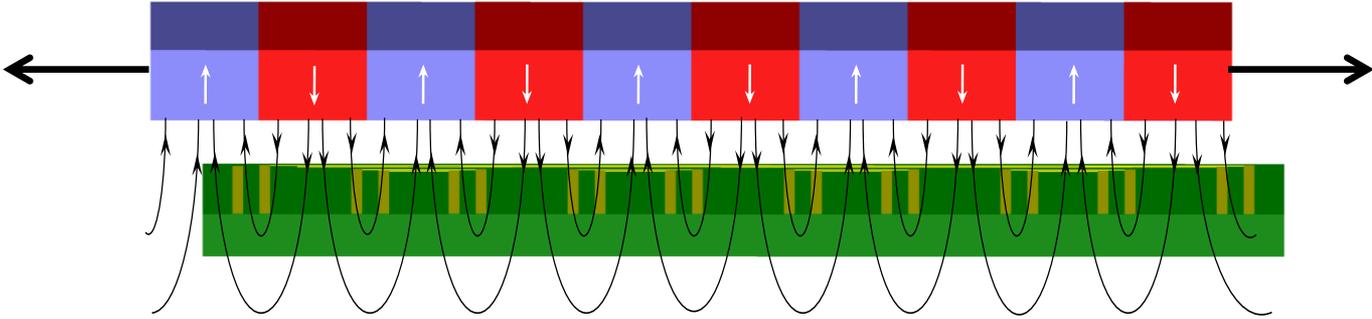


Developed for EcoHarvester. Design published in Roundy and Takahashi, Sensors and Actuators, 2013

Objectives

- Create (and understand) an energy harvesting transducer for a light switch that is
 - Planar and thin
 - Cheap
 - Highly efficient
 - Leverages new magnetic sheet manufacturing technology

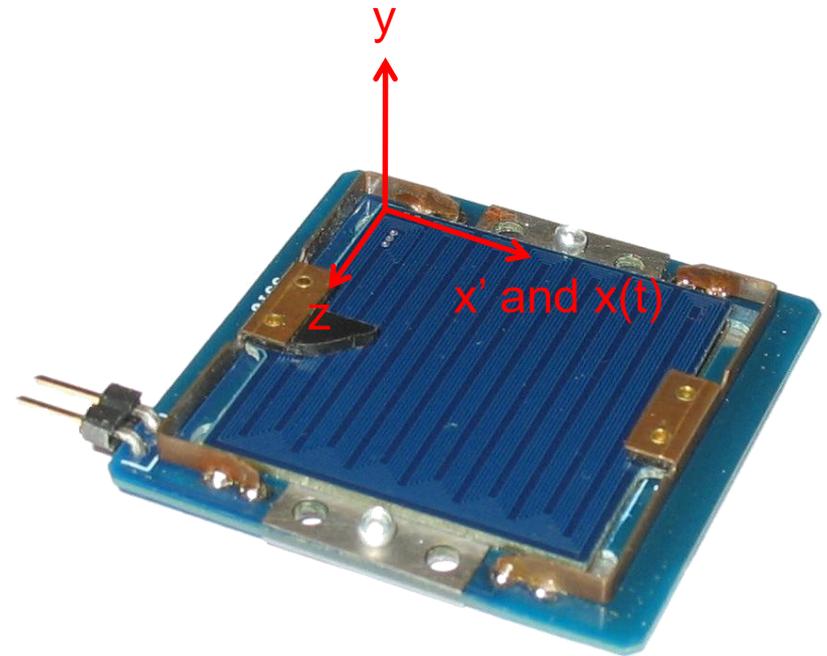


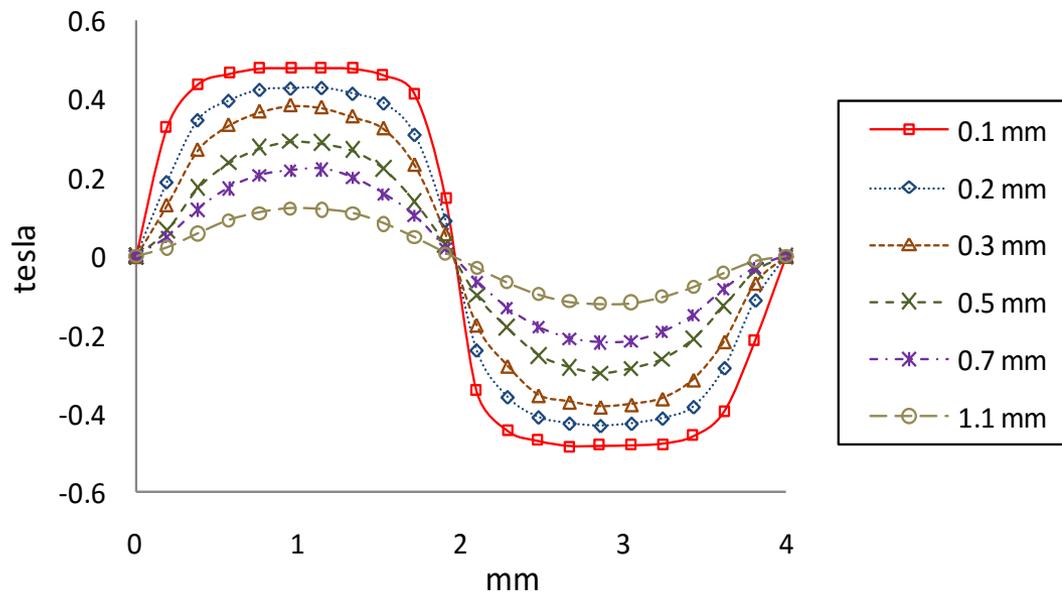
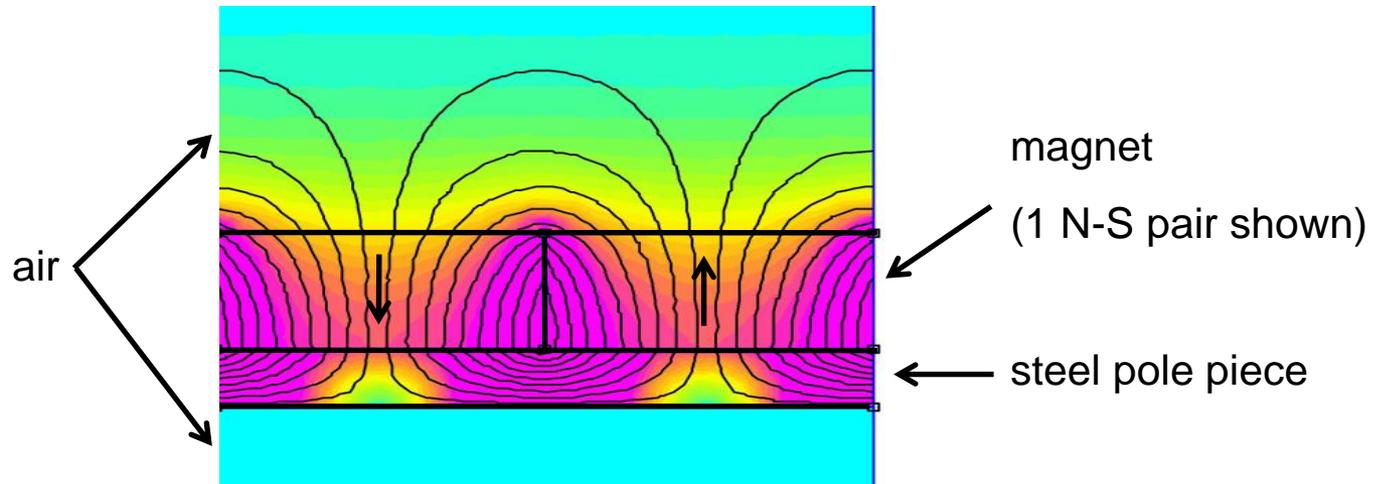


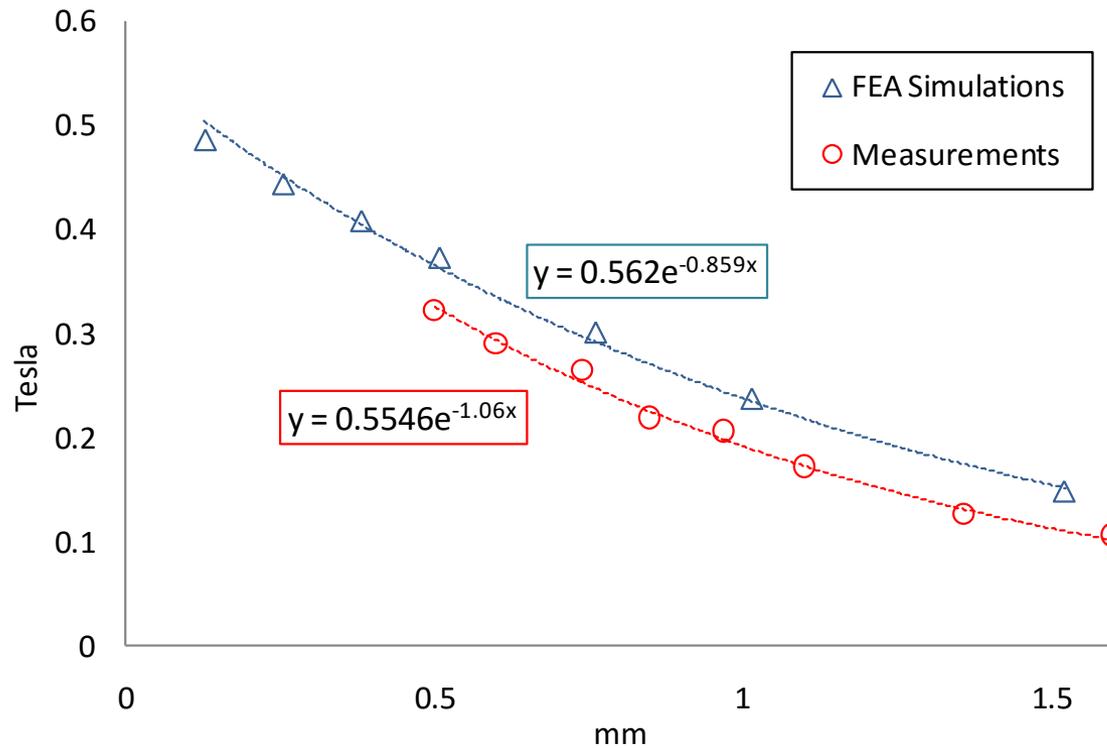
$$\frac{di}{dt} = -\frac{R + R_c}{L} i + \frac{1}{L} V_s$$

$$V_s = -\frac{d\Phi}{dt} = -Nl \frac{d}{dt} \left(\int_{x'}^{x''} B_y(x') dx' \right)$$

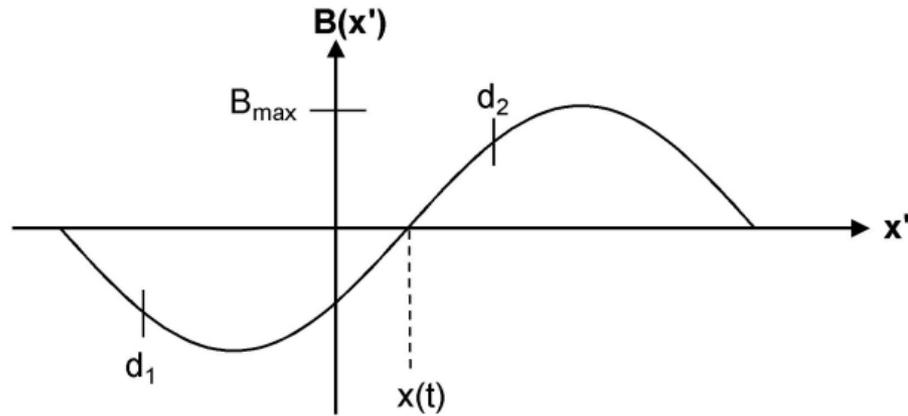
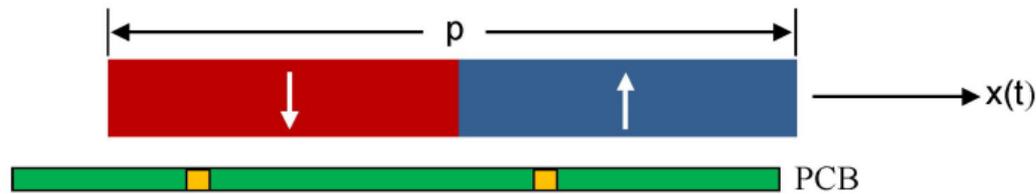
$$m\ddot{x} + b\dot{x} + N(\vec{l} \times \vec{B}) + kx = F_{in}(t)$$







$$B_y(x') = B_{\max} e^{-\alpha y(i)} \sin\left(\frac{2\pi}{p}(x' - x(t))\right)$$

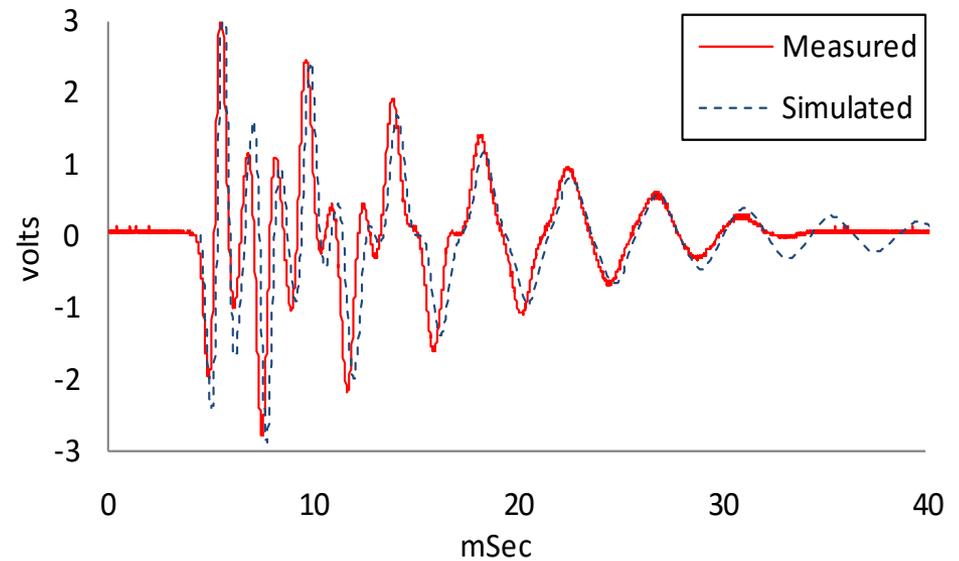


$$\frac{d\Phi}{dt} = NI \frac{d}{dt} \left(\int_{x'_1}^{x'_2} B_y(x') dx' \right)$$

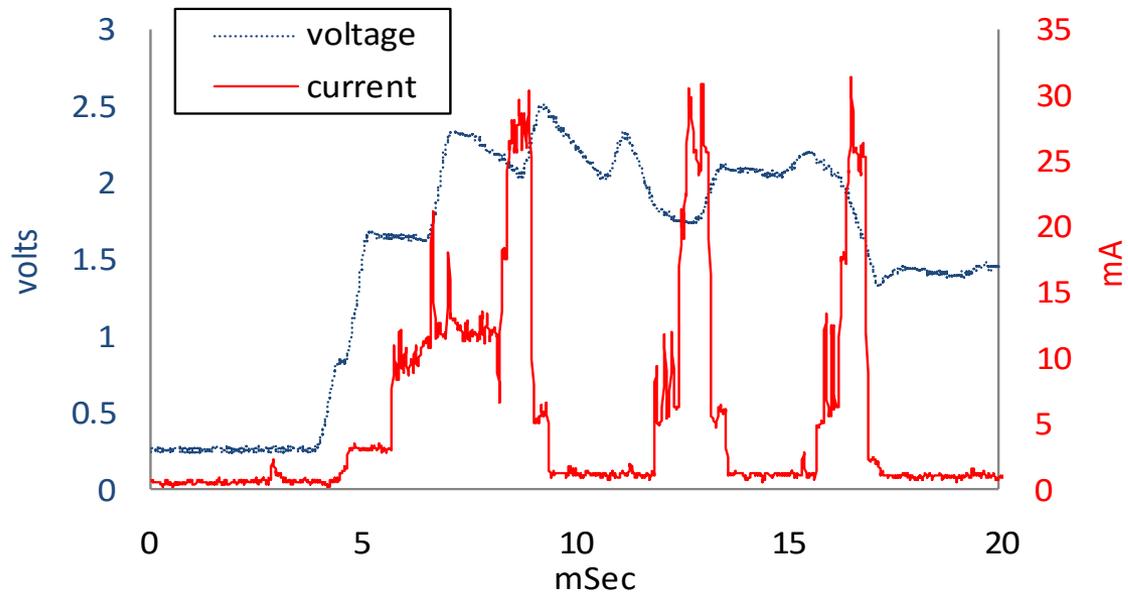
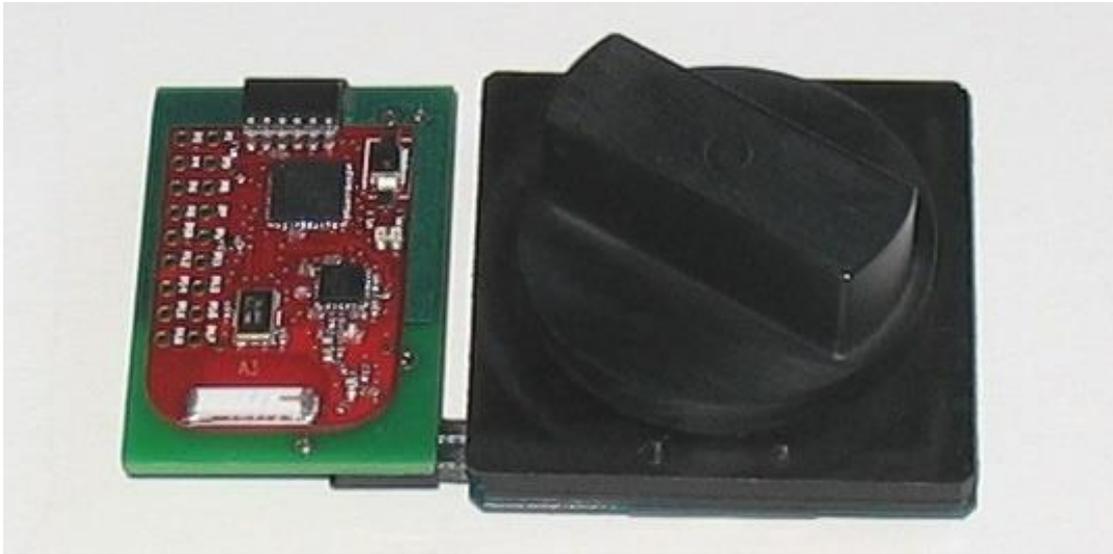
$$\frac{d\Phi}{dt} = NI B_{\max} e^{-\alpha y(i)} \dot{x} \left\{ \left[\sin\left(\frac{2\pi d_2}{p}\right) - \sin\left(\frac{2\pi d_1}{p}\right) \right] \cos\left(\frac{2\pi}{p} x(t)\right) - \left[\cos\left(\frac{2\pi d_2}{p}\right) - \cos\left(\frac{2\pi d_1}{p}\right) \right] \sin\left(\frac{2\pi}{p} x(t)\right) \right\}$$

d_1, d_2 refer to lateral position of conductors for a given coil.

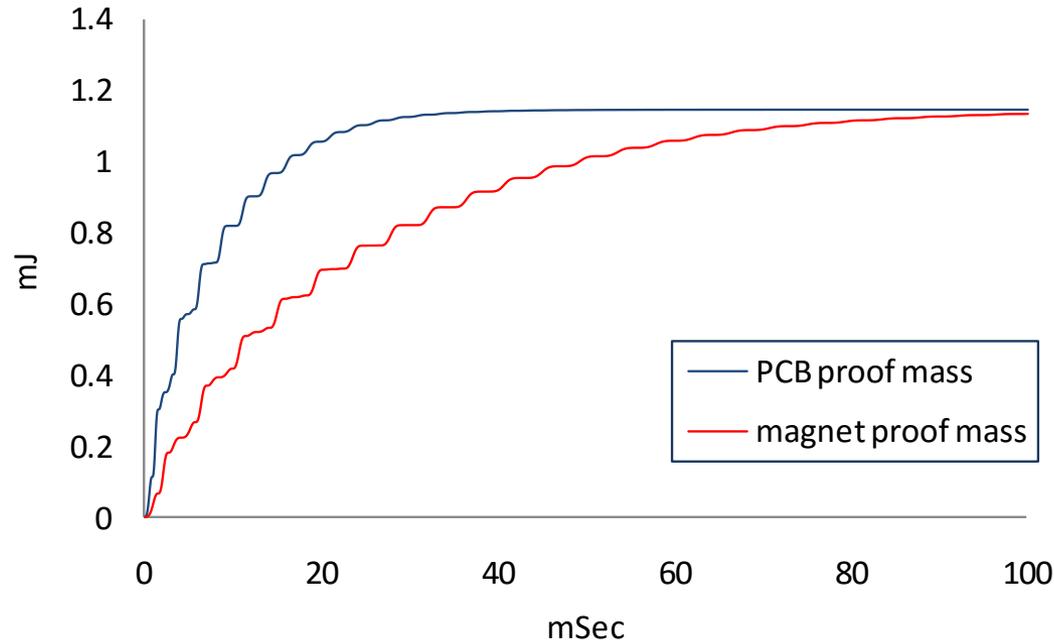
$y(i)$ refers to the distance from the magnet surface of the i^{th} layer



- Input displacement of 2mm (12 N max force, 12 mJ input)
- 1.1 mJ output per actuation
- 9% efficiency

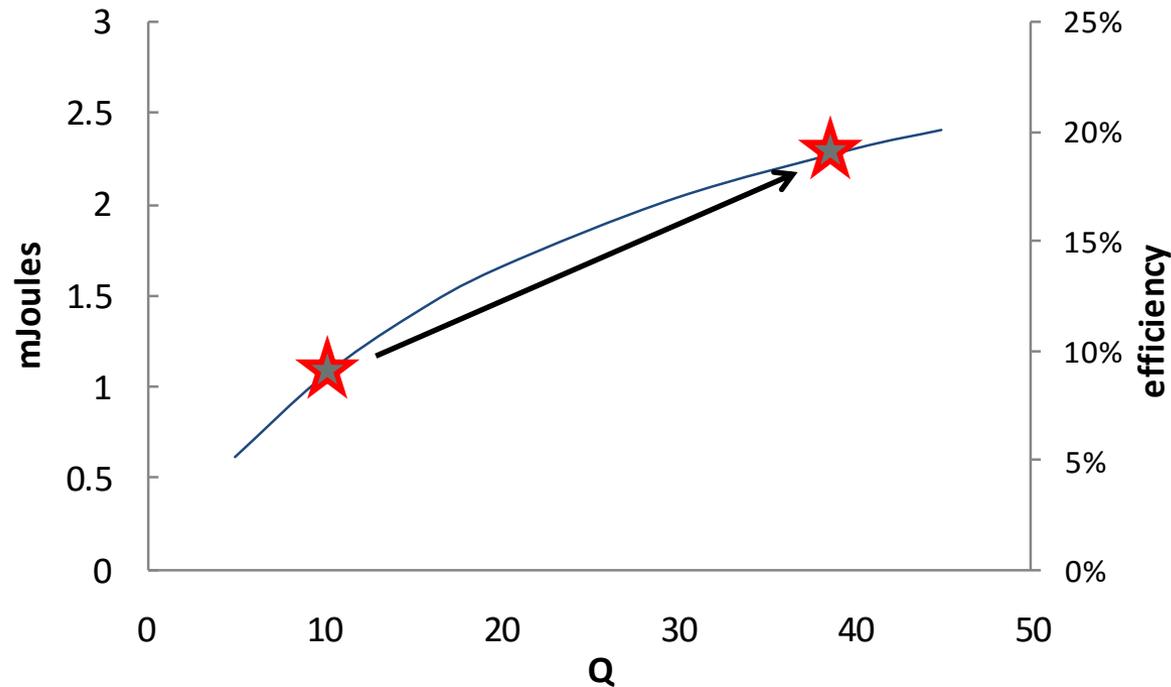


Magnet Vs. PCB as Proof Mass



- Total energy generated is the same
- Lighter proof mass generates energy faster with higher initial voltages
- Heavier proof mass rings down slower, generates for a longer time

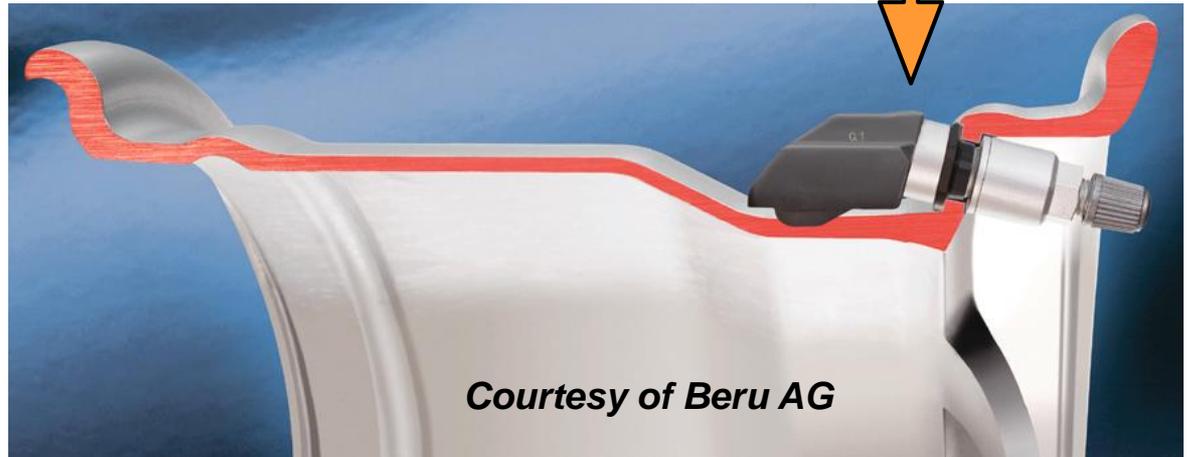
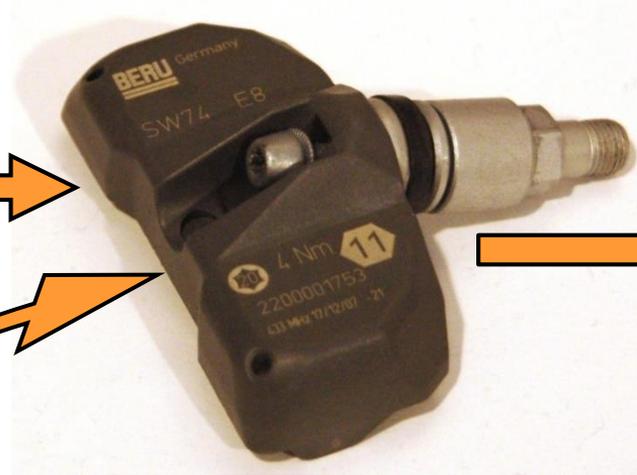
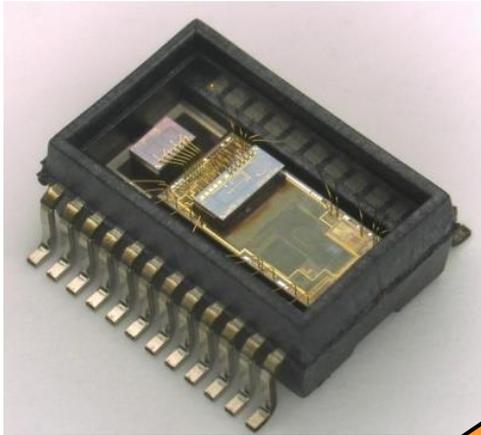
Energy vs. Mechanical Q



- We're operating at a total Q of just over 10.
- Effective Q from electromagnetic coupling is 65.
- Improved mechanical design could roughly double energy output.

TIRE PRESSURE MONITORING SYSTEMS

Tire Pressure Sensing Module

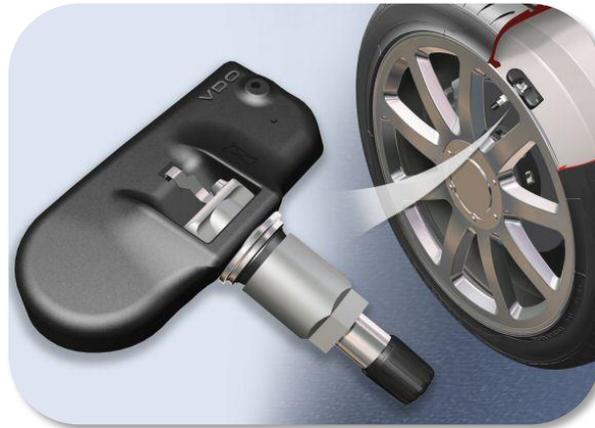
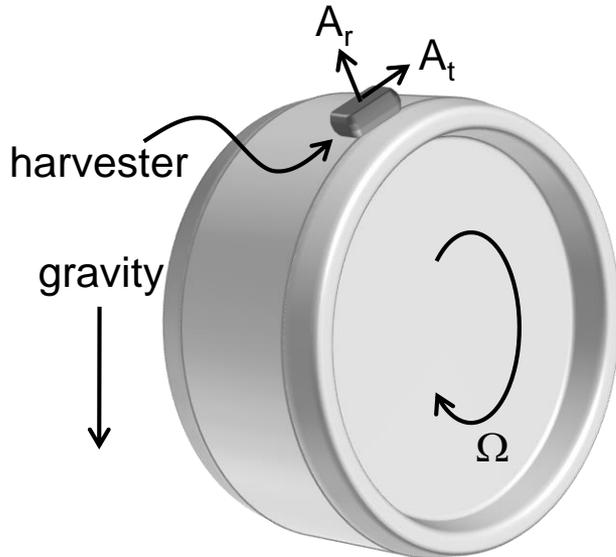


What's Wrong With A Battery?

- Concerns With Batteries
 - Limited Lifetime
 - Life Requirement Is 10 Years
 - Will Batteries Last?
 - Concerns At Temperature Extremes
 - High Internal Resistance At -40 C
 - Reliability At +125 C
 - Expensive
 - Cost ~ \$0.50
 - Polluting
 - But This Isn't A Really Big Application In The Battery World

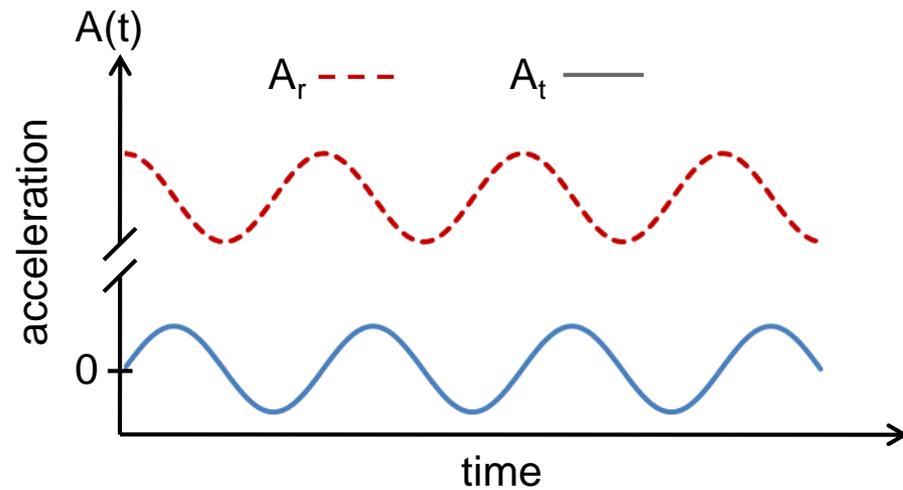
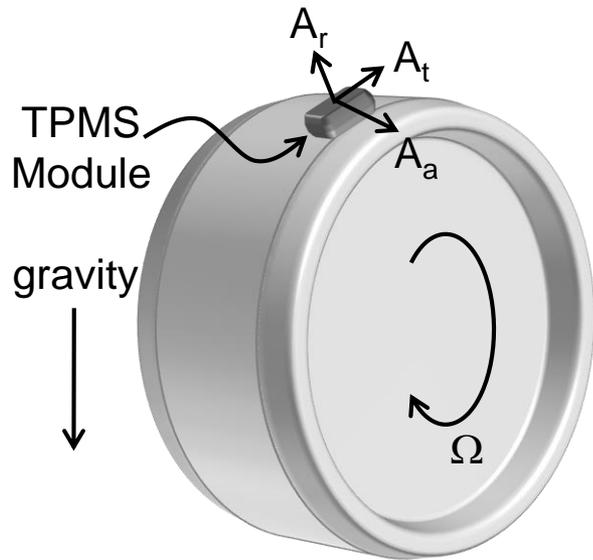


The Energy Harvesting Problem

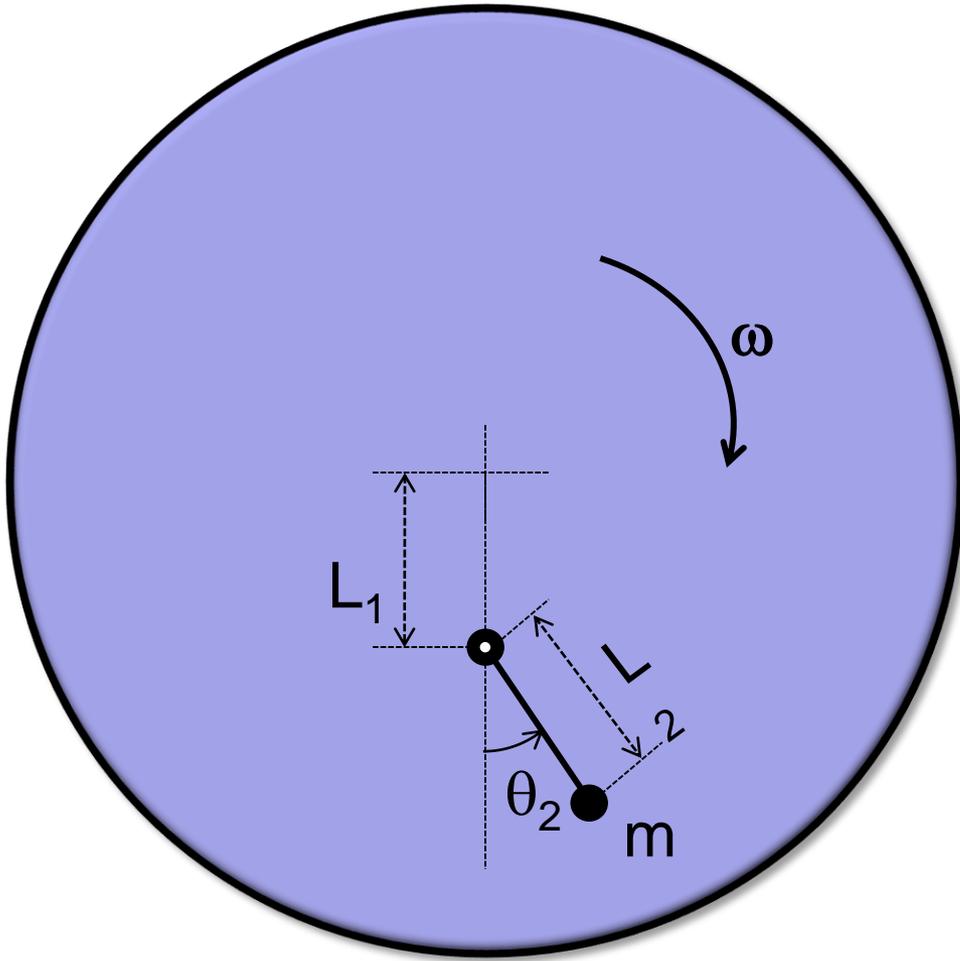


- Three critical requirements drove our solution
 - First transmission within first 100 tire revolutions, no rechargeable battery
 - During regular driving must transmit at least once per minute – corresponds to at least 20 μW power generation
 - Low profile

Acceleration Signals

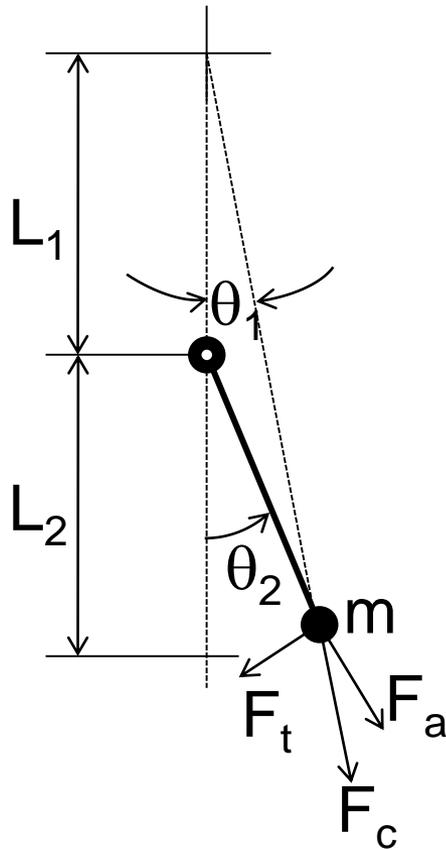


Self-tuning Pendulum System



- Pendulum located on rotating wheel or disc offset from center
- Centripetal acceleration will tend to straighten pendulum
- Restoring torque on mass (m) is a function of angular displacement (θ_2)
- Looks like a spring

Self-tuning Pendulum System



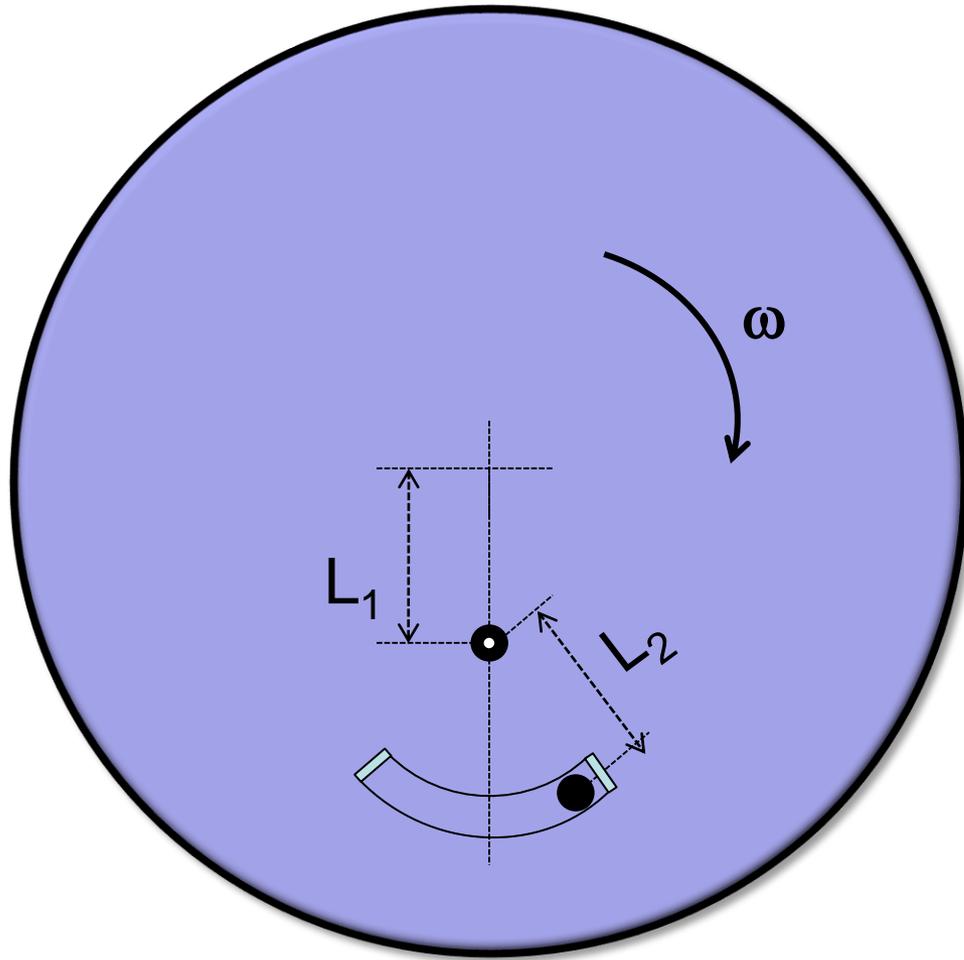
Rotational inertia $I = mL_2^2$

Torque on pendulous mass $\tau = F_t L_2 = m\omega^2 L_1 L_2 \theta_2$

Effective rotational stiffness $K_\theta = \frac{\partial \tau}{\partial \theta_2} = m\omega^2 L_1 L_2$

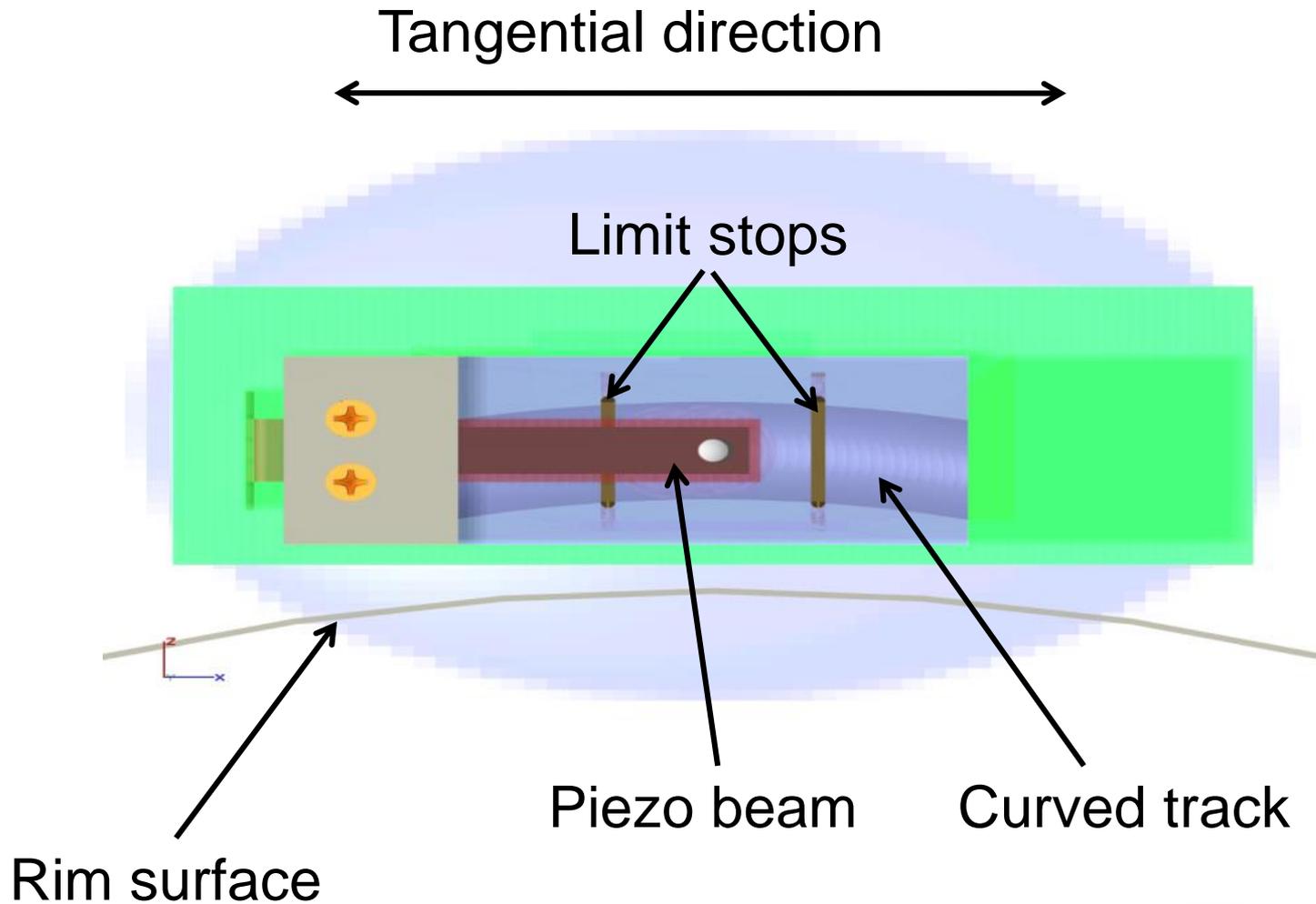
Pendulum resonant frequency $\omega_n = \sqrt{\frac{K_\theta}{I}} = \omega \sqrt{\frac{L_1}{L_2}}$

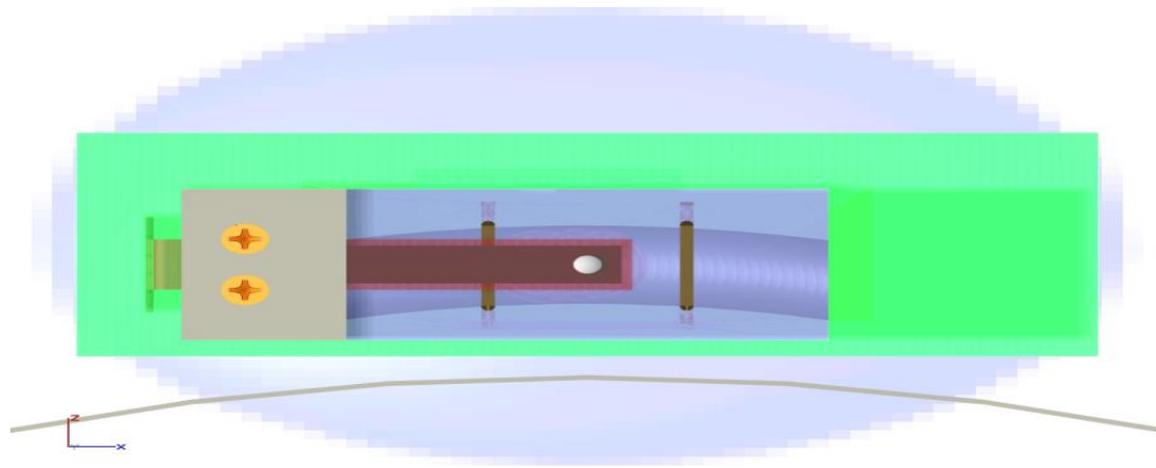
Self-tuning Track System



- Pendulum is not practical for a car tire
- Track with radius of L_2 and center of rotation L_1 from wheel center performs same function

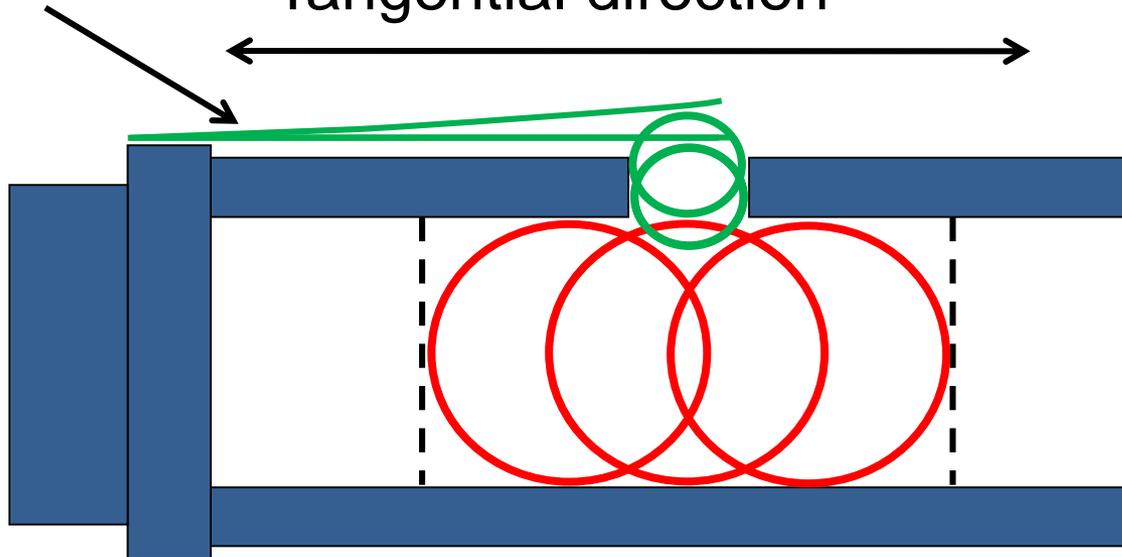
Prototype Concept



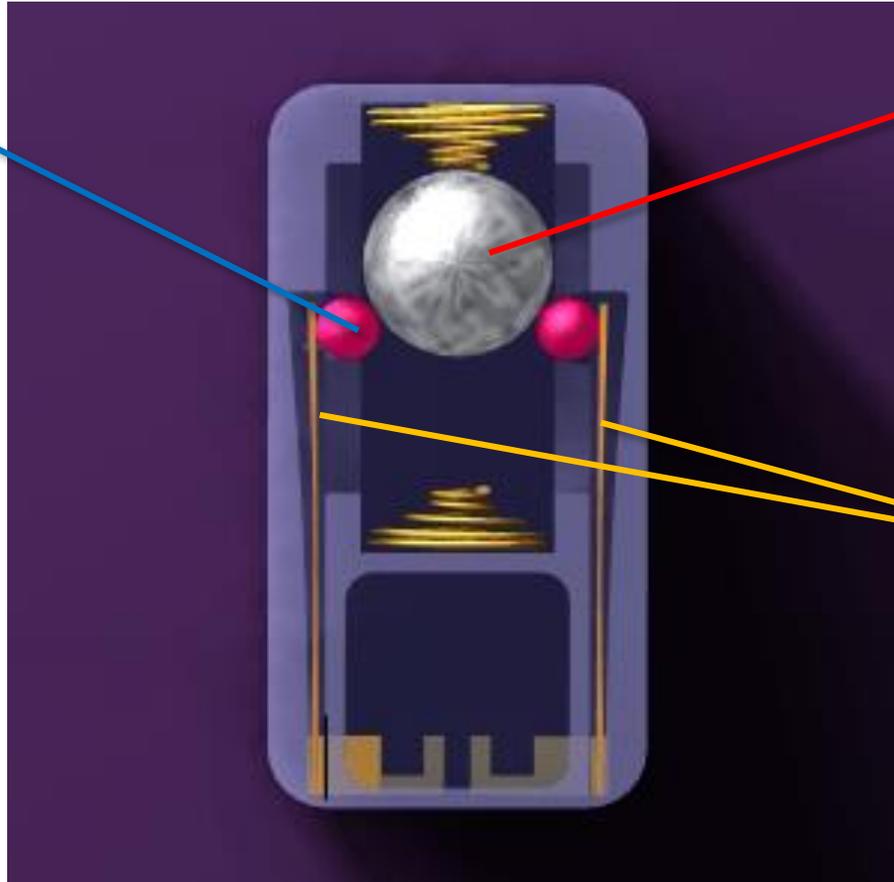


Piezo beam

Tangential direction

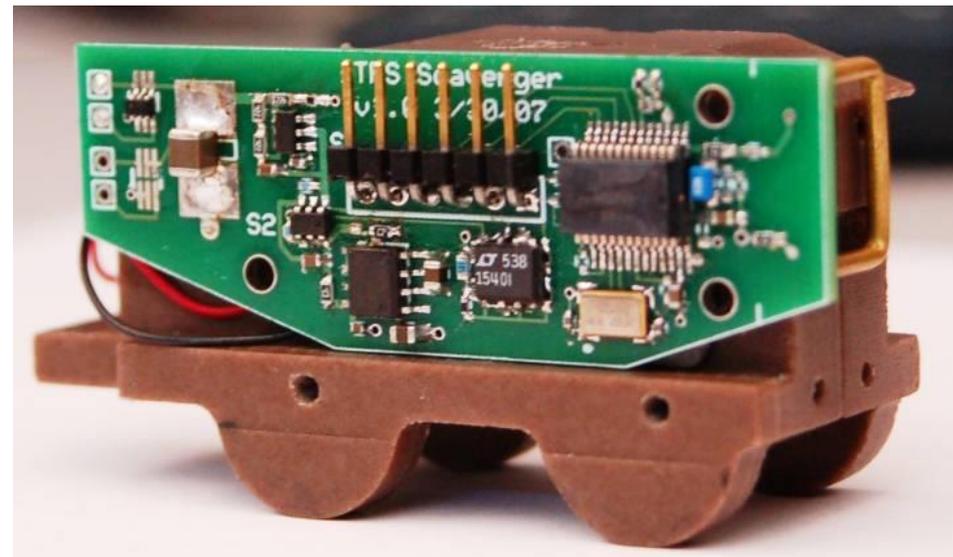
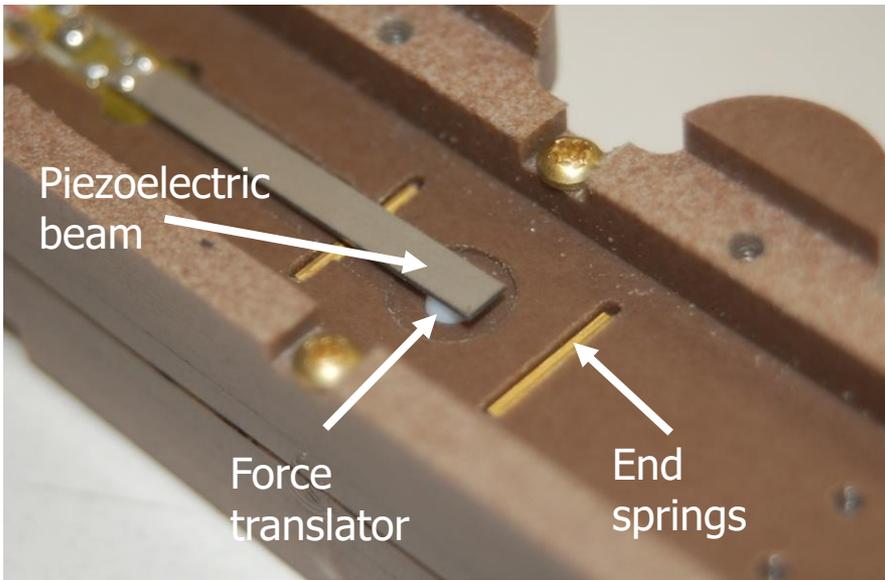
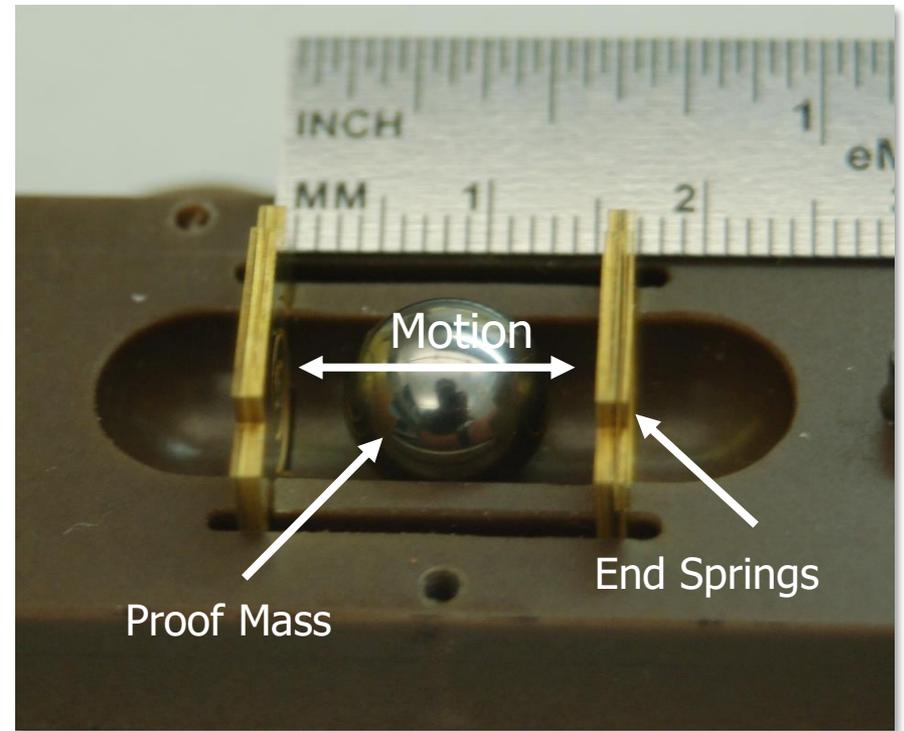
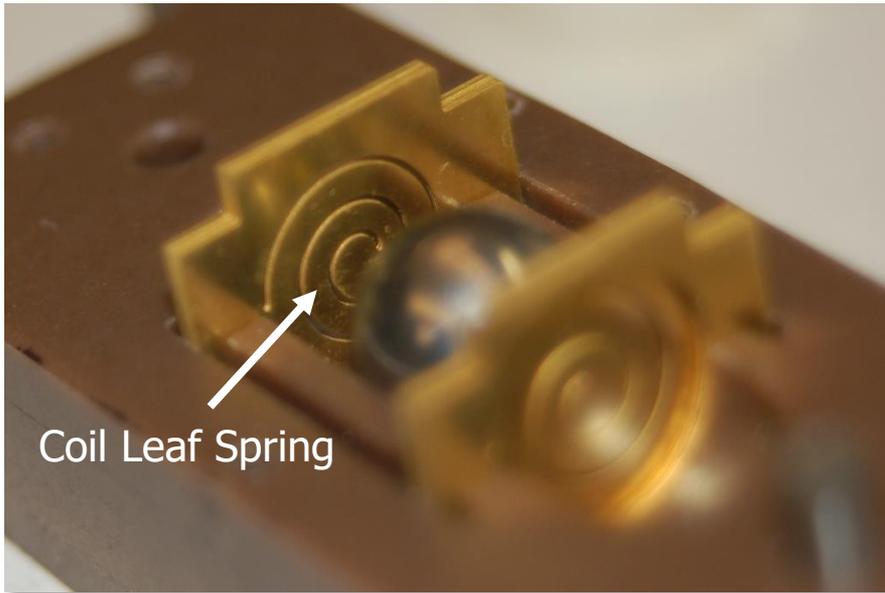


Force
Translator

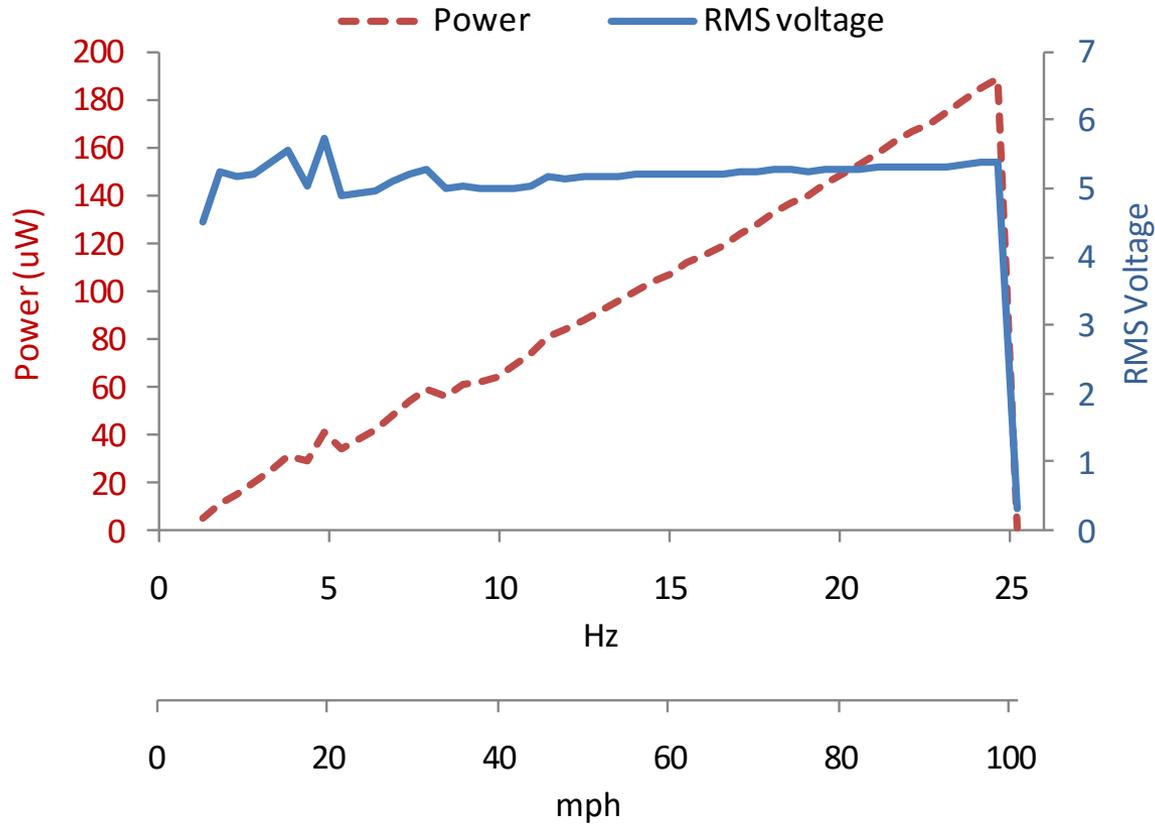


Proof
Mass

Piezo
Beams

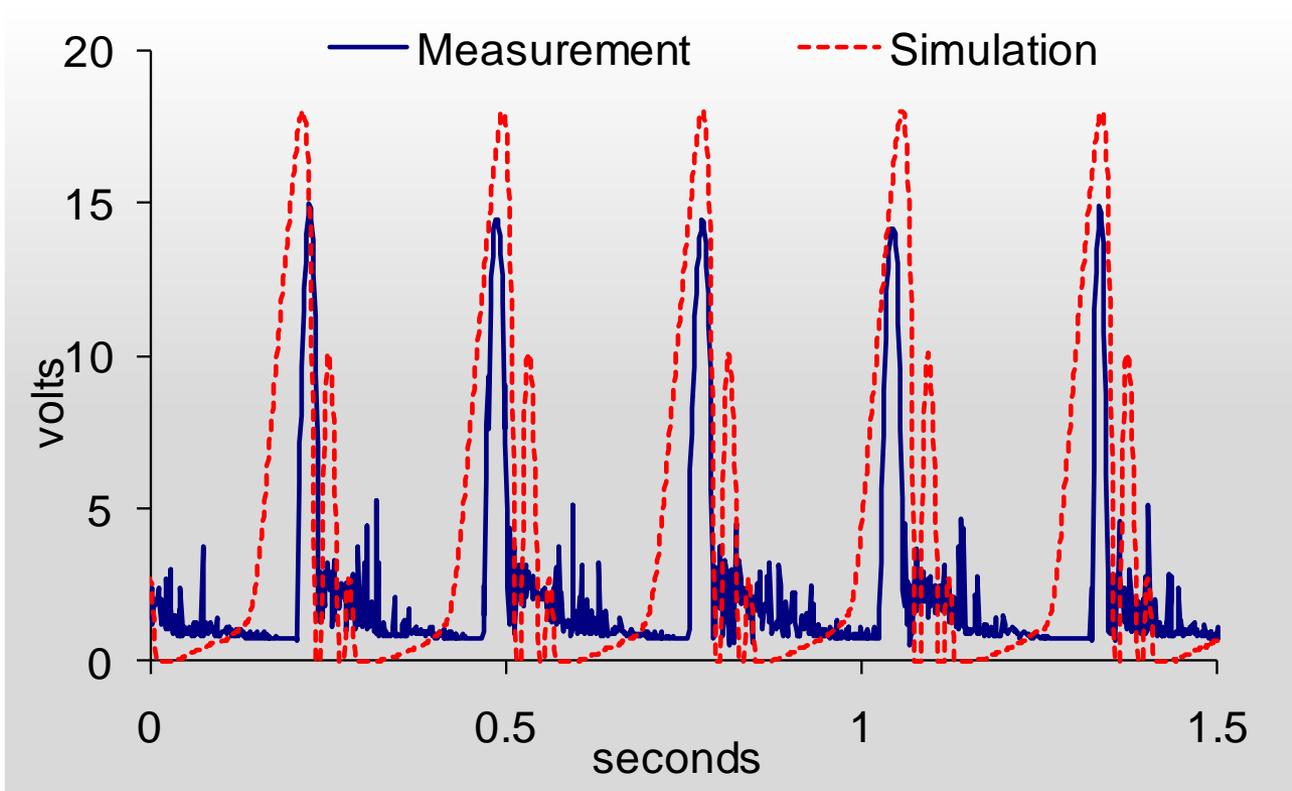


Simulation Output



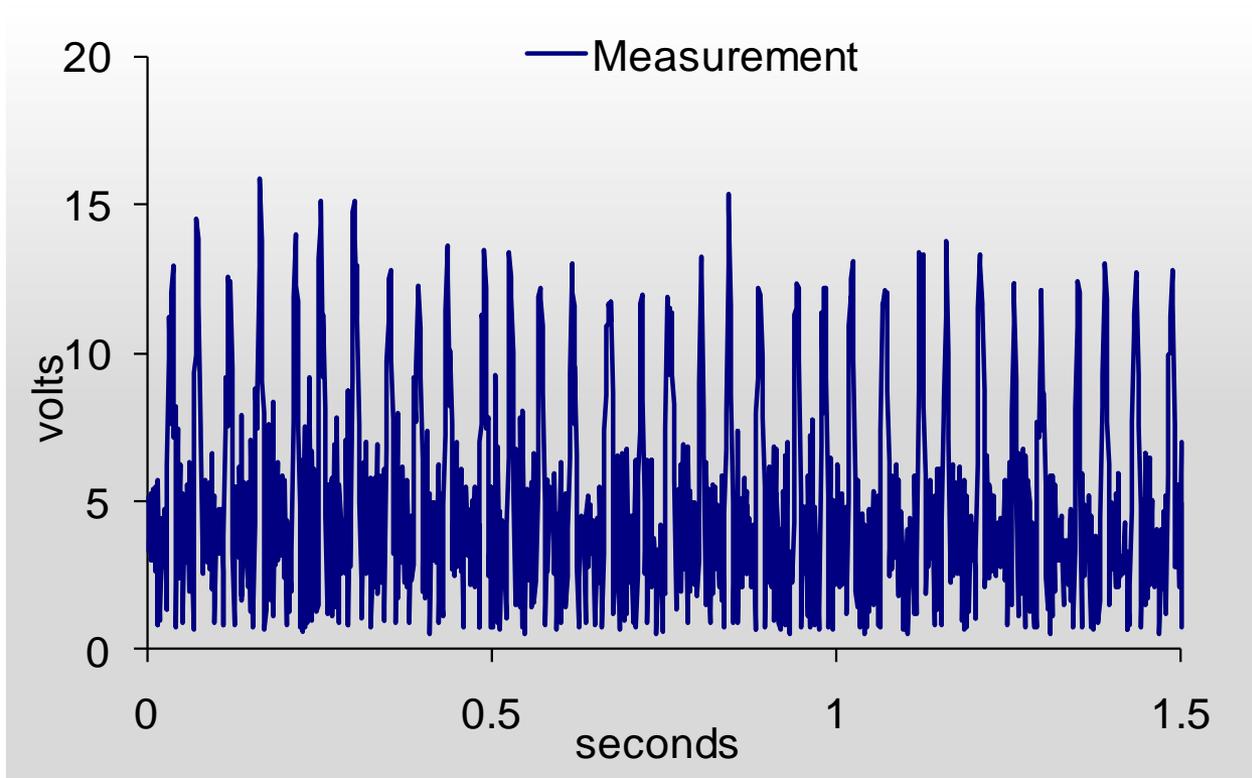
Test Stand Results

10 mph



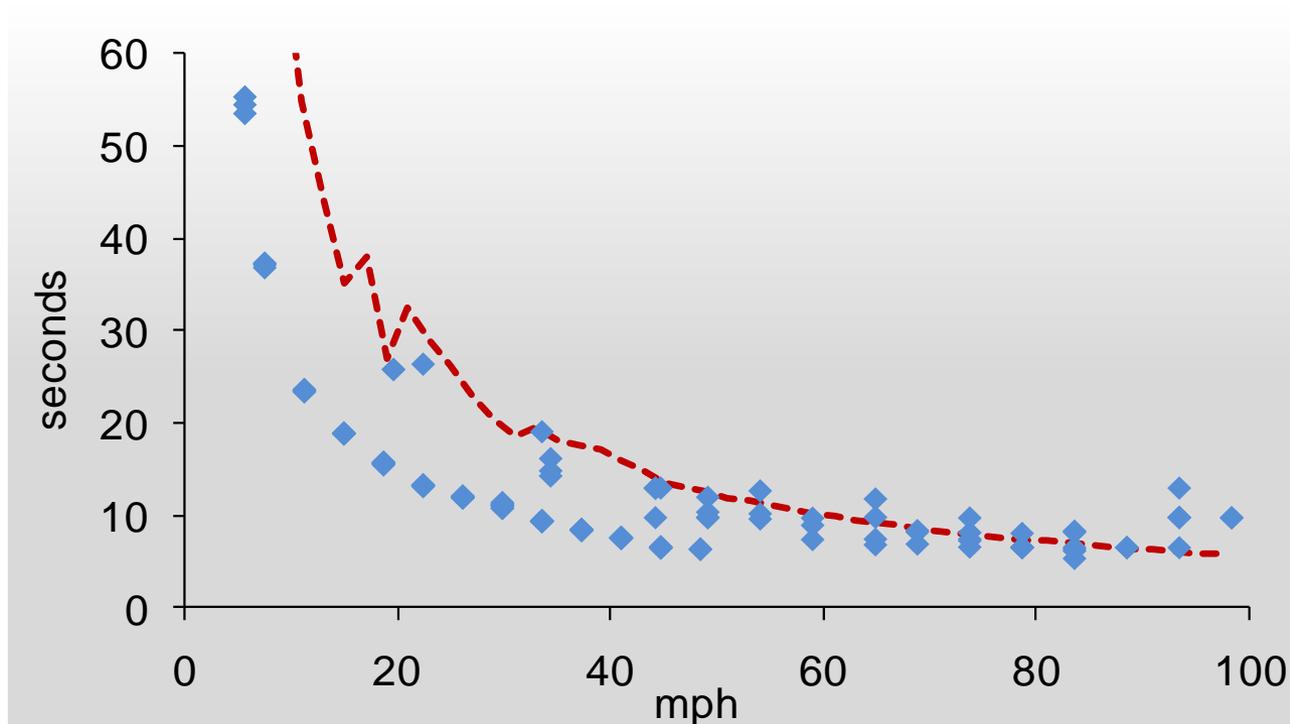
Test Stand Results

55 mph



Road Test Results

Time Between Transmissions



ENERGY HARVESTING FOR WEARABLES

Heel Strike - Shoes

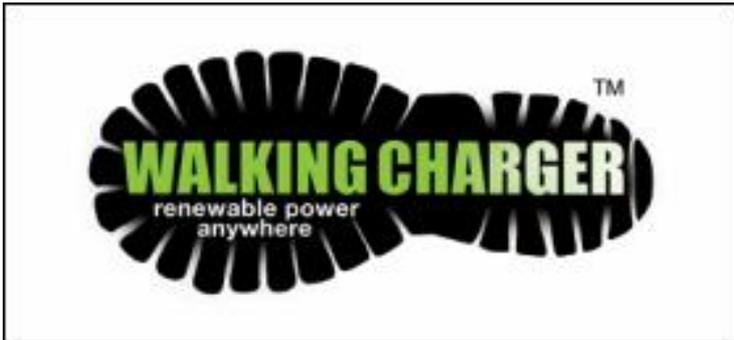


Krupenkin and Taylor. 2011 Nature Communications

Claim 1 watt nominal power

See also <http://www.instepnanopower.com/>

Heel Strike - Shoes



<http://www.energyharvesters.com/>

Claim 1 watt nominal power (also)

Underlying technology does not seem to be disclosed

And, many others like this



Inertial Harvesters Worn on Body

Status and Activity Buttons

Hold the left button to check the battery level, or hold the right button and shake to watch AMPY generate power.

Inductor Technology

Two of AMPY's inductors transform your movement into usable power for your devices.

Dual-Charging Ports

Charge up your devices from your AMPY's USB port just as fast as any wall outlet. You can also use your AMPY like any other battery and charge it from any USB outlet.



Form-Fitting / Sweatproof Body

The AMPY MOVE form was designed to match the curves of your body, resulting in a comfortable form-fit feel. The outer surface is finished with a soft-touch, sweat-proof finish, making it perfect for any workout.

1800 mAH Li-Ion Battery

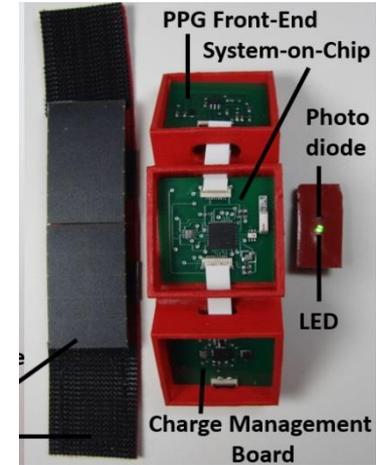
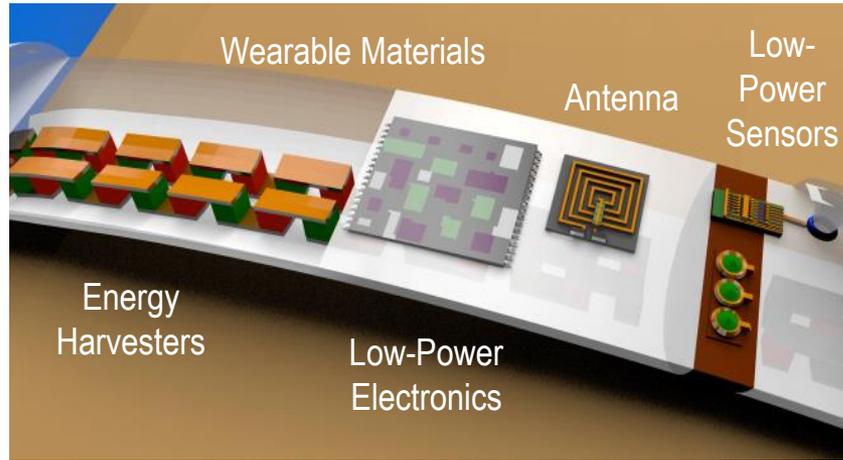
The AMPY MOVE has a 1800mAh battery, which is enough to fully charge an iPhone 6.

- <http://www.getampy.com/>
- “An hour of exercise can produce up to 1 hour smart phone battery life.”
- My own testing falls very far short of this.

Inertial Harvesters Worn on Body



Energy Harvesting for Wearables



- Clearly a big market where power sources are important
- What role can / will inertial energy harvesting play?



Standard Quartz Watch

< 10 μ W



Jawbone UB4

- Battery: 38 mAh, 3.6 v = 137 J
- Lasts “up to 7 days”.
- 225 – 500 μ W average power draw



APPLE WATCH



APPLE WATCH SPORT

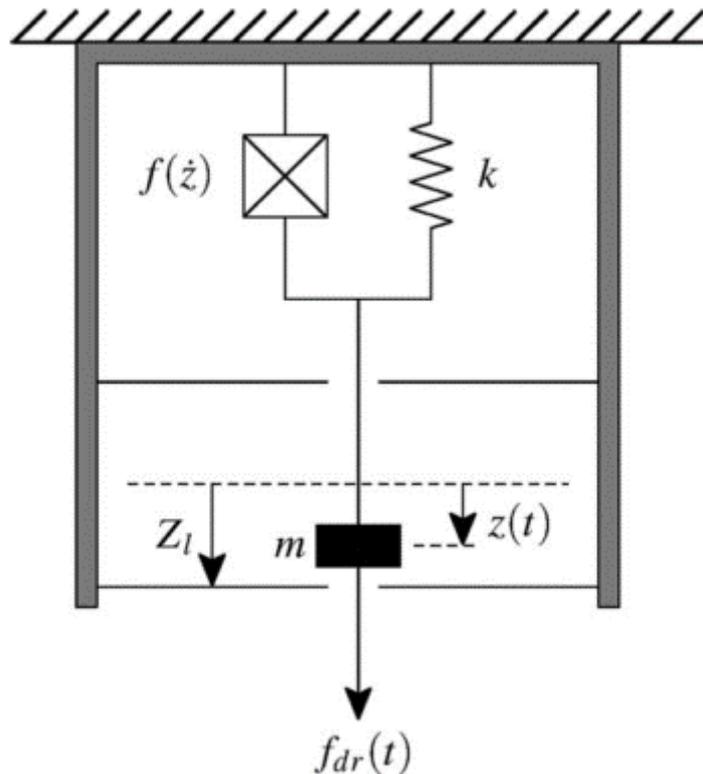


APPLE WATCH EDITION

Apple Watch (38 mm version)

- Battery: 205 mAh, 3.6 V = 738 J
- Lifetime: 5 – 18 hrs \rightarrow 14 - 41 mW
- 14 – 41 mW average power draw

How Much Potential Power Is There?



$$P_{max} = \frac{2}{\pi} Y_0 Z_l \omega^3 m$$

Y_0 = excitation amplitude (m)

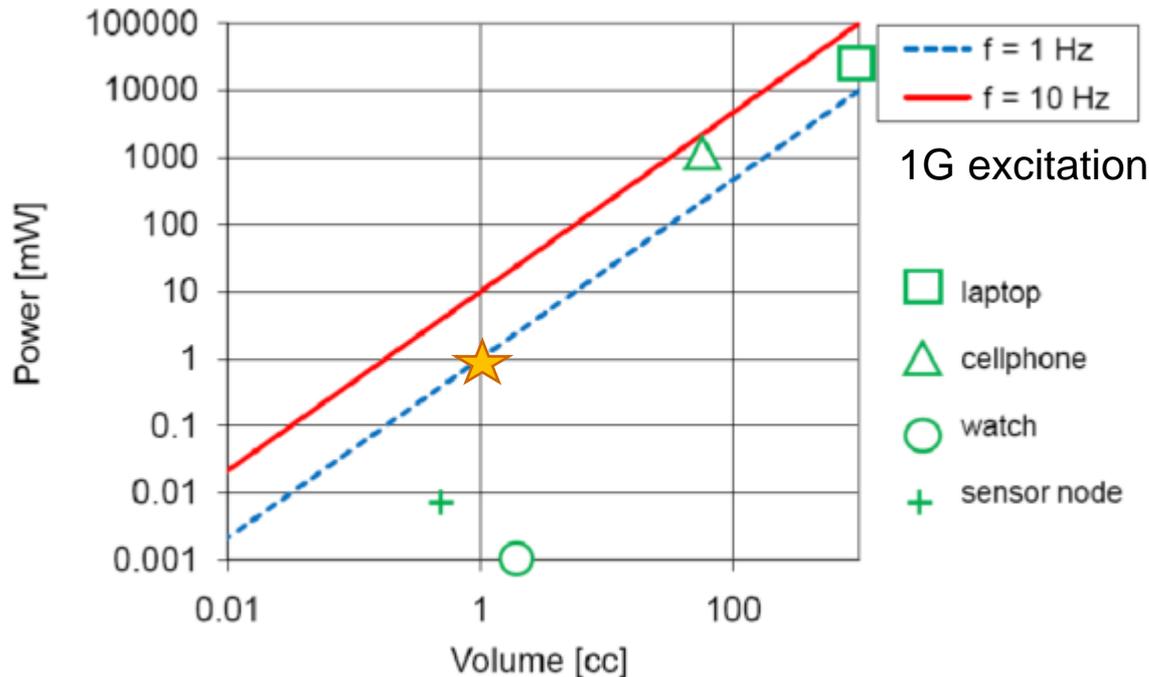
Z_l = maximum proof mass motion range (m)

ω = excitation frequency (rad/s)

m = proof mass (kg)

Mitcheson, P.D.; et. al. "Energy Harvesting From Human and Machine Motion for Wireless Electronic Devices," in *Proceedings of the IEEE*, vol.96, no.9, pp.1457-1486, Sept. 2008

How Much Potential Power Is There?



- Linear proof mass motion
- Proof mass density = 20 g/cc
- ½ available space taken by proof mass
- Transducer takes no space
- Proof mass motion is “optimally damped”
- 1G continuous excitation

Rotation Based Energy Harvesters

Kinetron generator in Swatch Autoquartz watch

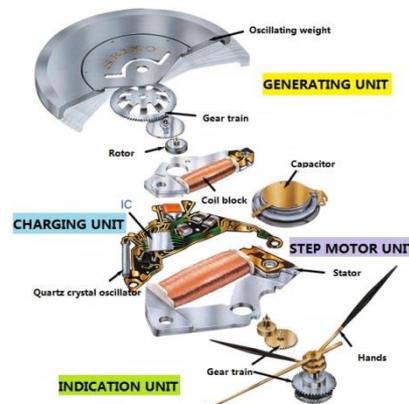


3D drawing of the MGS Watch

400 mJ/day
9.3 μ W ave (12 hr day)

Kinetron data sheet

Seiko Kinetic watch

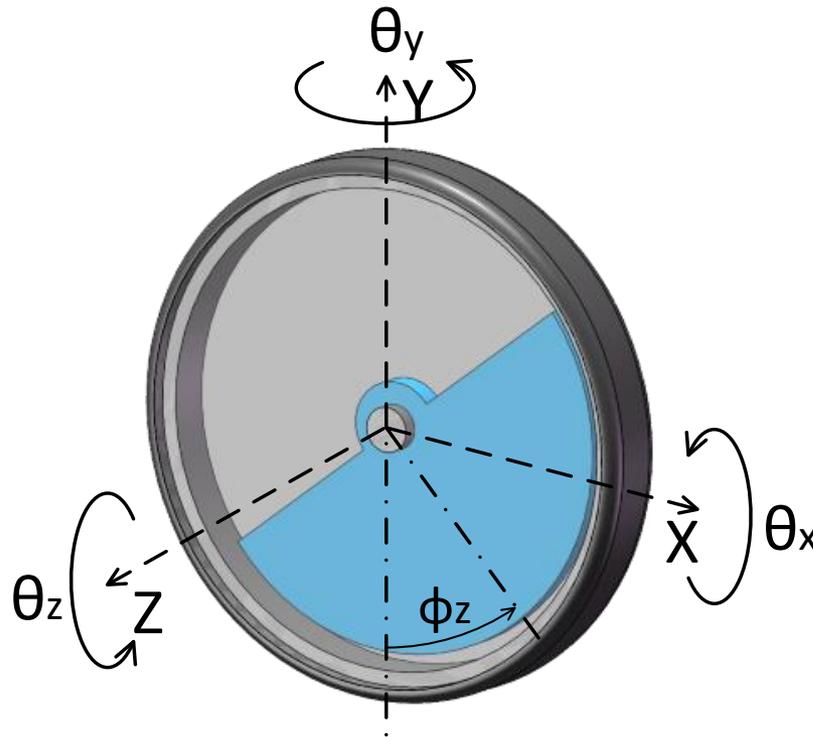


5-10 μ W average

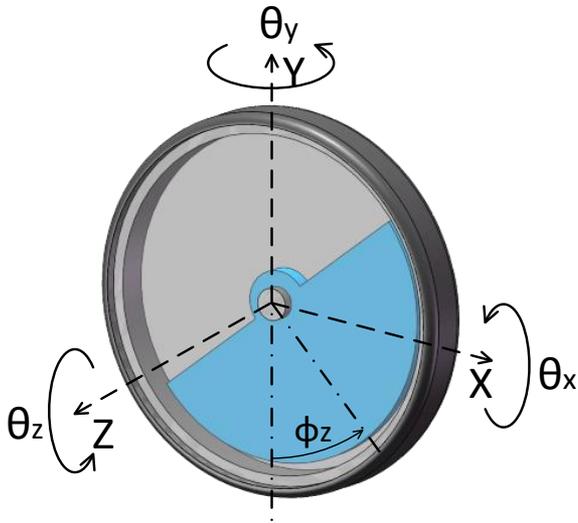
Mitcheson, 2010

Paradiso and Starner, 2005

Theoretical Maximum Power



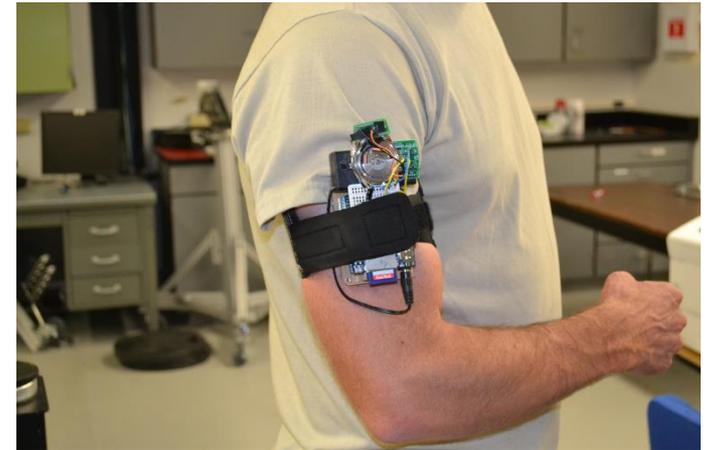
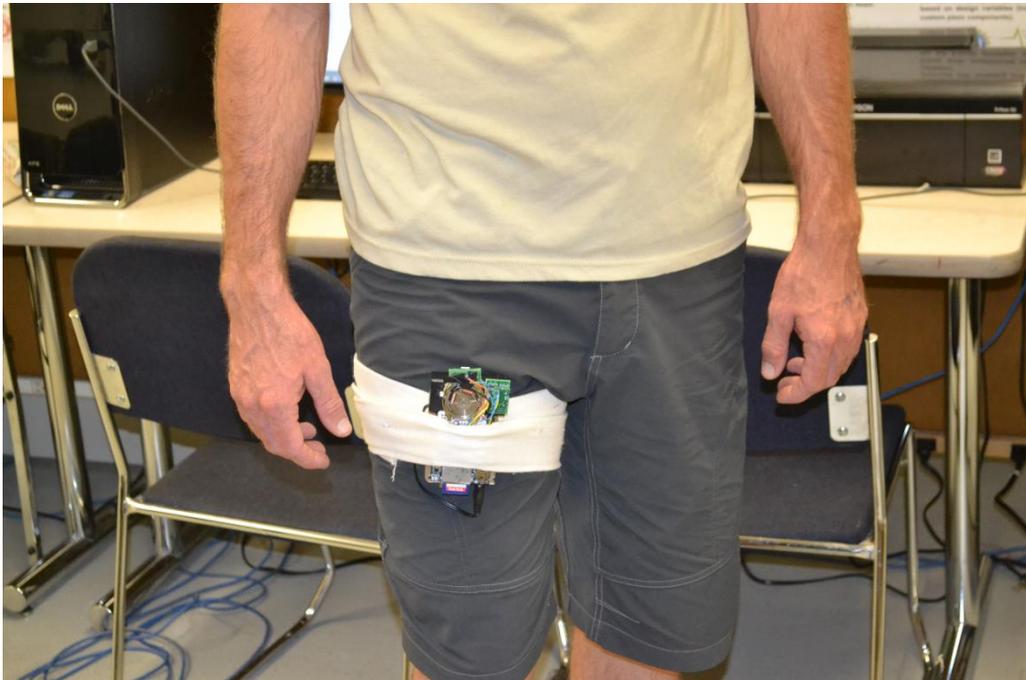
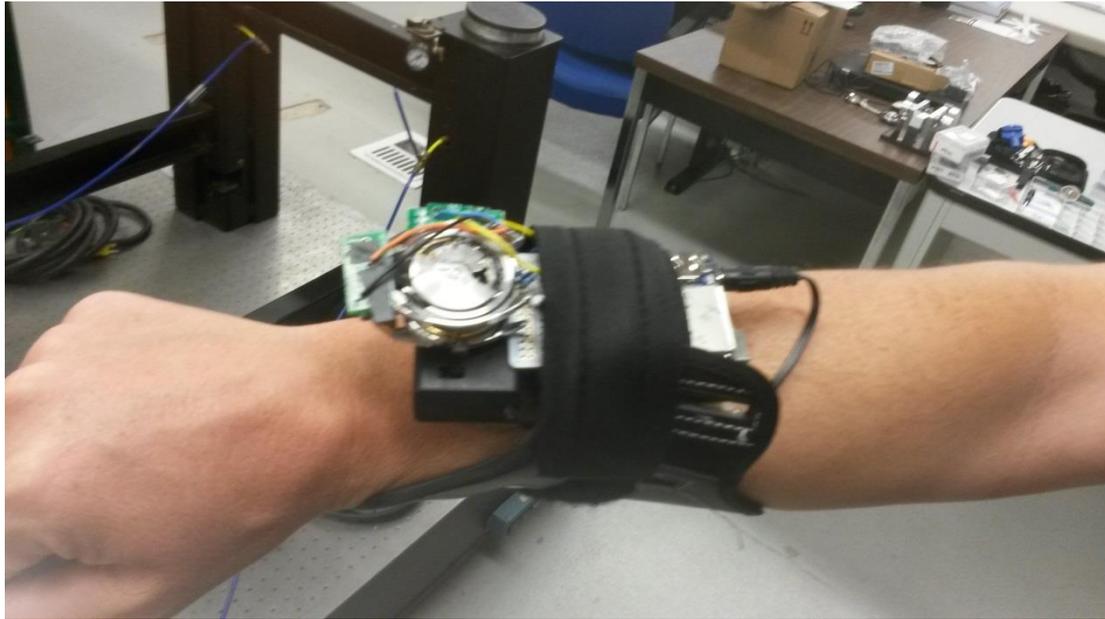
Theoretical Maximum Power



$$m \begin{bmatrix} -l \cos \phi_z \cdot \dot{\phi}_z^2 - l \sin \phi_z \cdot \ddot{\phi}_z \\ -l \sin \phi_z \cdot \dot{\phi}_z^2 + l \cos \phi_z \cdot \ddot{\phi}_z \end{bmatrix} = -m \begin{bmatrix} \ddot{X} \\ \ddot{Y} \end{bmatrix} + \begin{bmatrix} F_x \\ F_y \end{bmatrix} + m \begin{bmatrix} g_x \\ g_y \end{bmatrix}$$

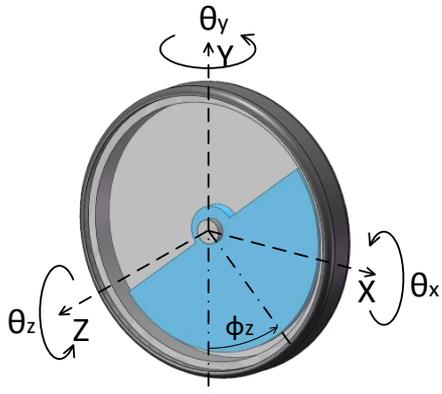
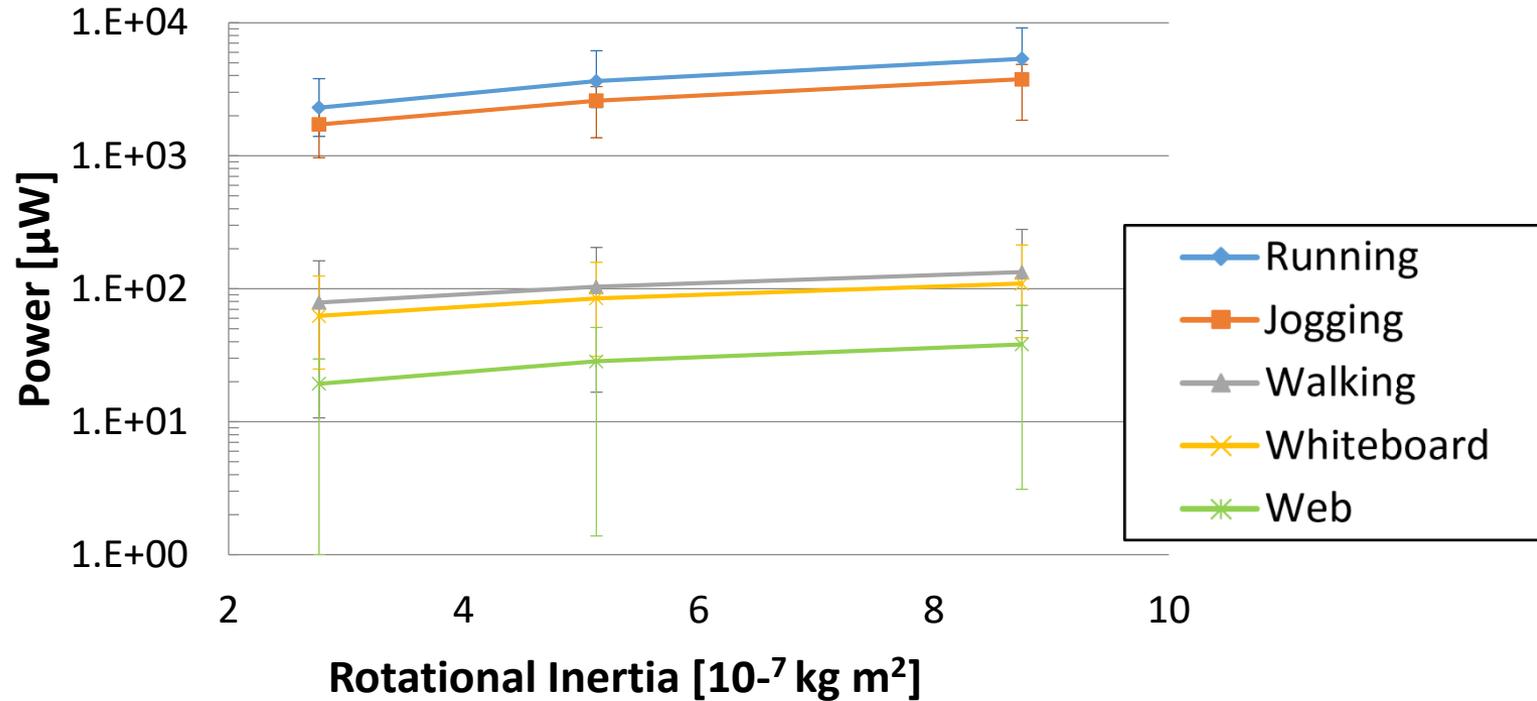
$$I_G (\ddot{\theta}_z + \ddot{\phi}_z) = -(D_e + D_m) \dot{\phi}_z + F_x l \sin \phi_z - F_y l \cos \phi_z$$

$$P = D_e \dot{\phi}_z^2$$



Theoretical Maximum Power

Wrist - Walking



$$m \begin{bmatrix} -l \cos \phi_z \cdot \dot{\phi}_z^2 - l \sin \phi_z \cdot \ddot{\phi}_z \\ -l \sin \phi_z \cdot \dot{\phi}_z^2 + l \cos \phi_z \cdot \ddot{\phi}_z \end{bmatrix} = -m \begin{bmatrix} \ddot{X} \\ \ddot{Y} \end{bmatrix} + \begin{bmatrix} F_x \\ F_y \end{bmatrix} + m \begin{bmatrix} g_x \\ g_y \end{bmatrix}$$

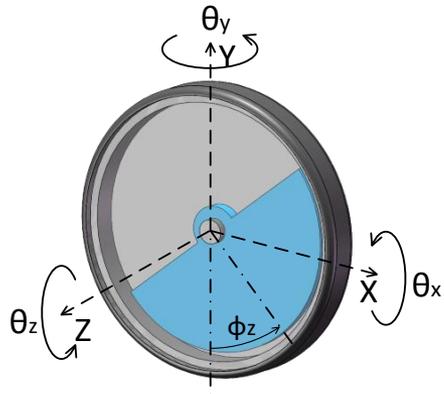
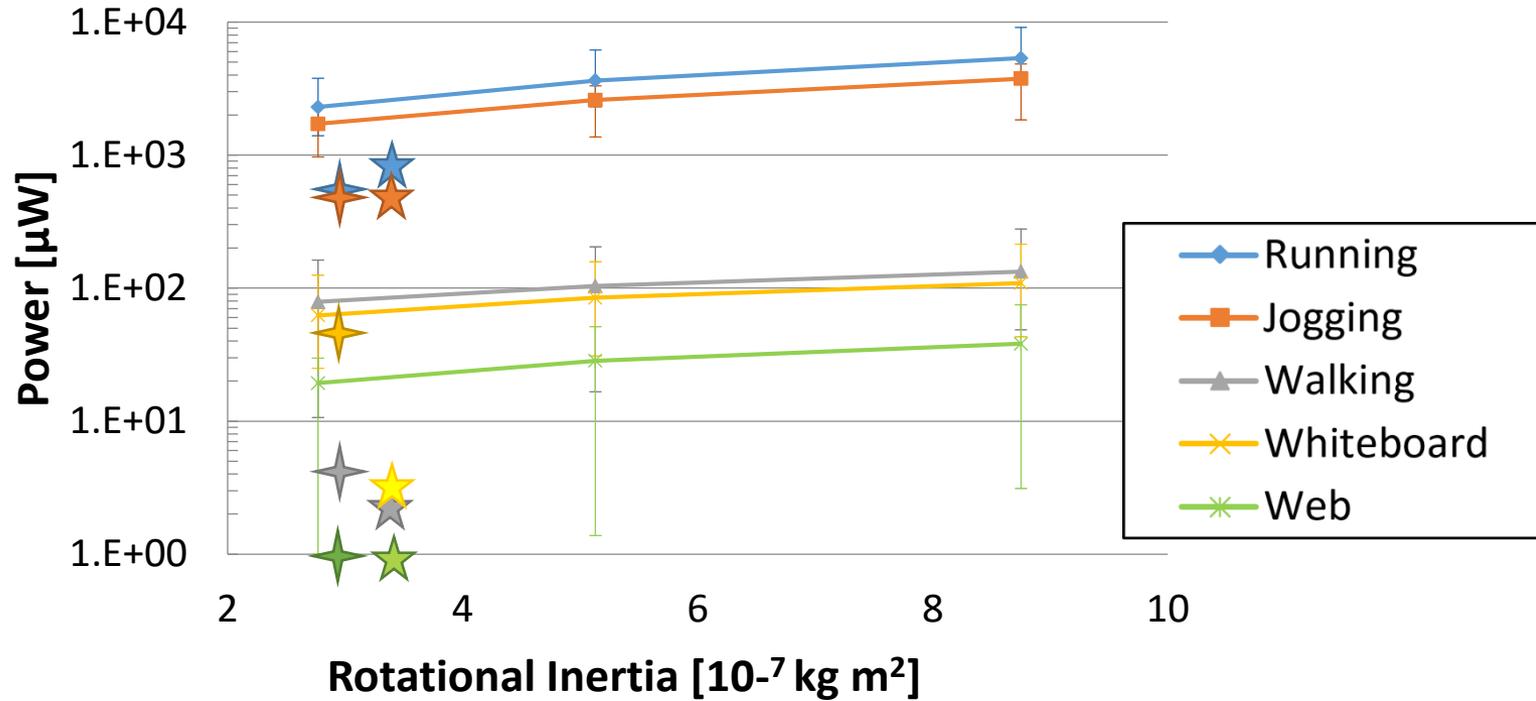
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$$P = D_e \dot{\phi}_z^2$$

Theoretical Maximum Power

Wrist - Walking

☆ Seiko
 ☆ Kinetron



$$m \begin{bmatrix} -l \cos \phi_z \cdot \dot{\phi}_z^2 - l \sin \phi_z \cdot \ddot{\phi}_z \\ -l \sin \phi_z \cdot \dot{\phi}_z^2 + l \cos \phi_z \cdot \ddot{\phi}_z \end{bmatrix} = -m \begin{bmatrix} \ddot{X} \\ \ddot{Y} \end{bmatrix} + \begin{bmatrix} F_x \\ F_y \end{bmatrix} + m \begin{bmatrix} g_x \\ g_y \end{bmatrix}$$

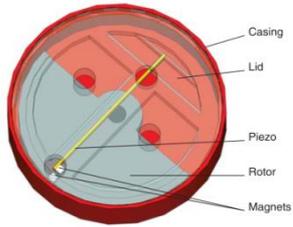
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$$P = D_e \dot{\phi}_z^2$$

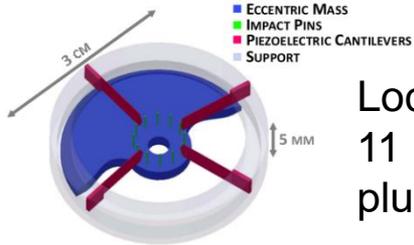
Where Is the Potential for Improvement?

- Watches have relatively high total (mechanical + electrical) damping with $D_e \gg D_m$
- Must overcome static friction / damping under low excitation to start generating much energy.
 - Underperform during walking.
- Other inefficiencies
 - 40% efficiency between energy stored in intermediate spring and electrical power output
- Don't take advantage of potentially beneficial dynamics (i.e. springs and resonance)

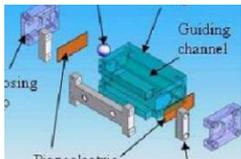
Theoretical Maximum Power



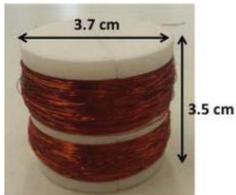
Pillatsch, et.al. 2013
7 μ W - Jogging



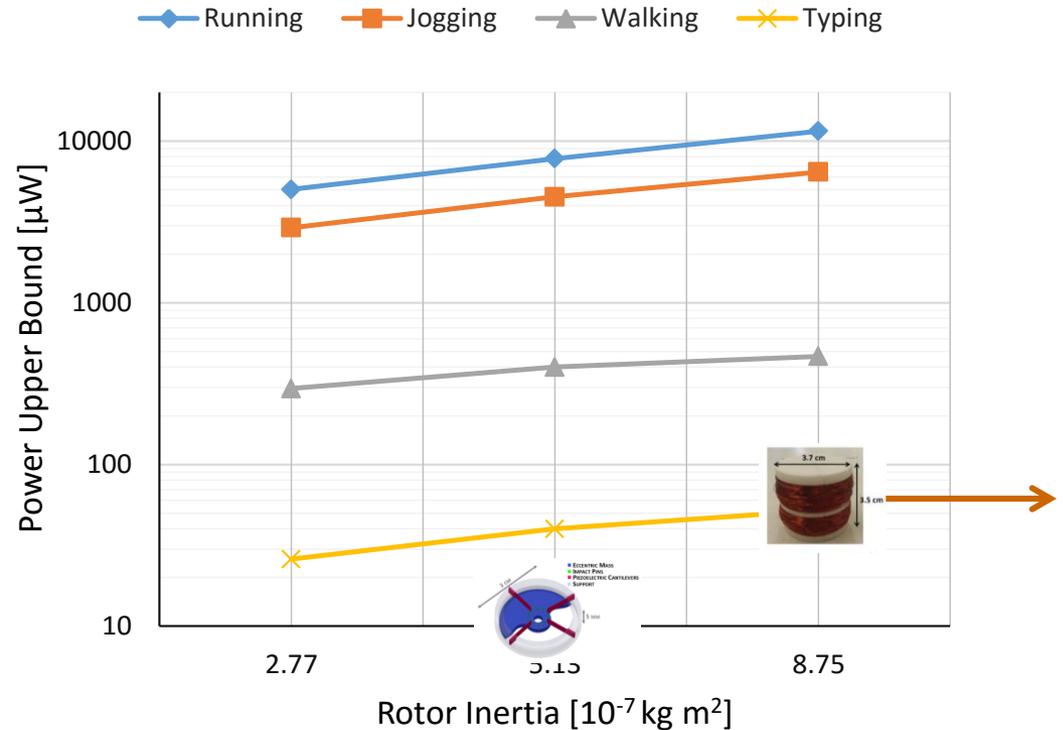
Lockhart, et.al. 2014
11 μ W – “Continuous plucking”



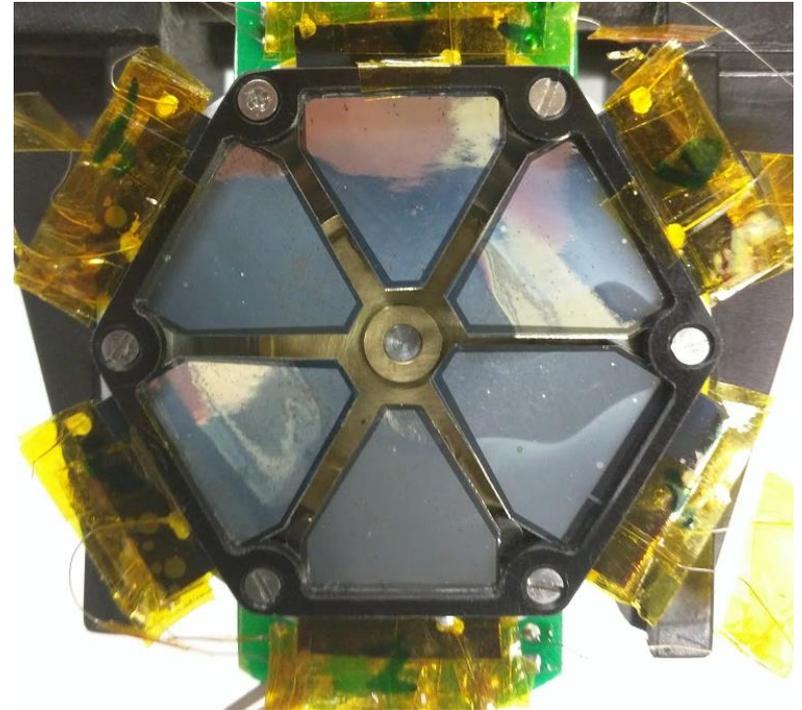
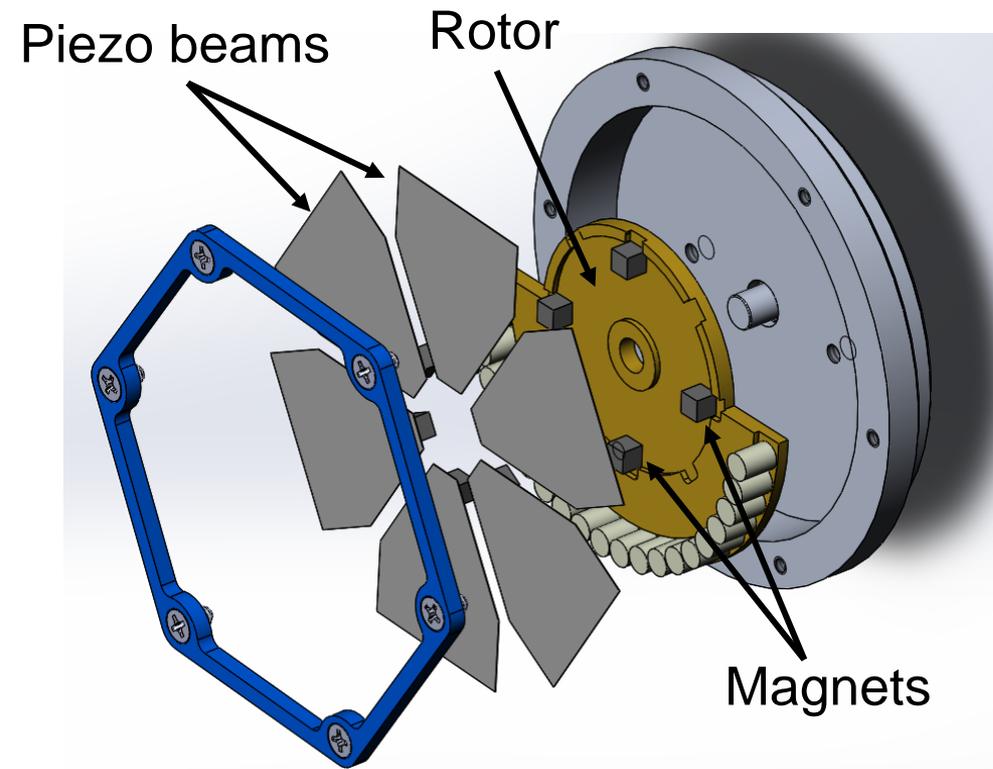
Renauld, et.al. 2009
47 μ W – “Continuous rotation”



Rao, et.al. 2013
100 μ W – jogging
33 μ W - walking

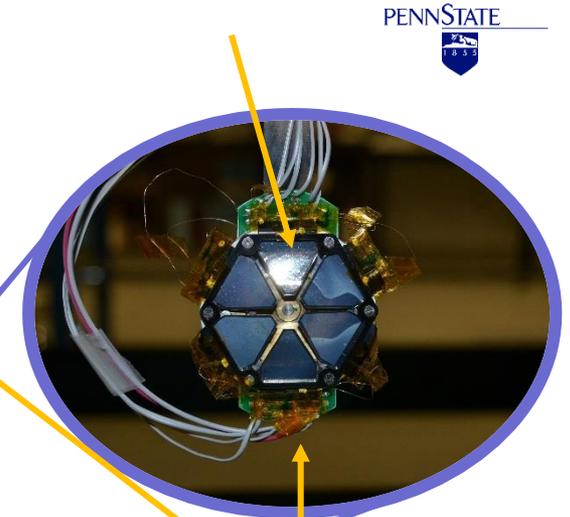
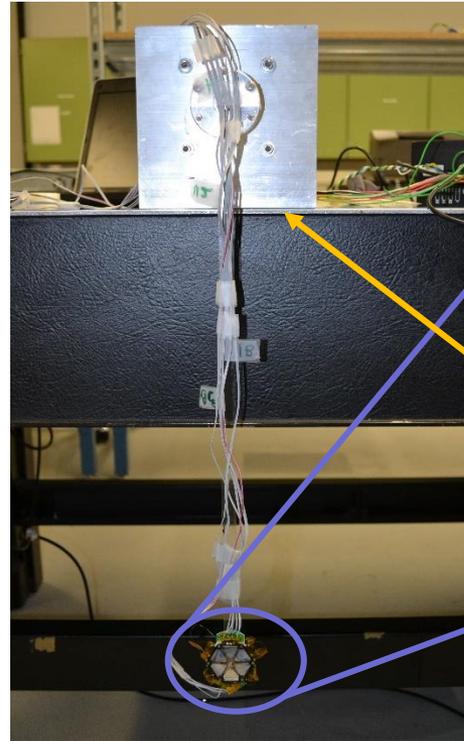
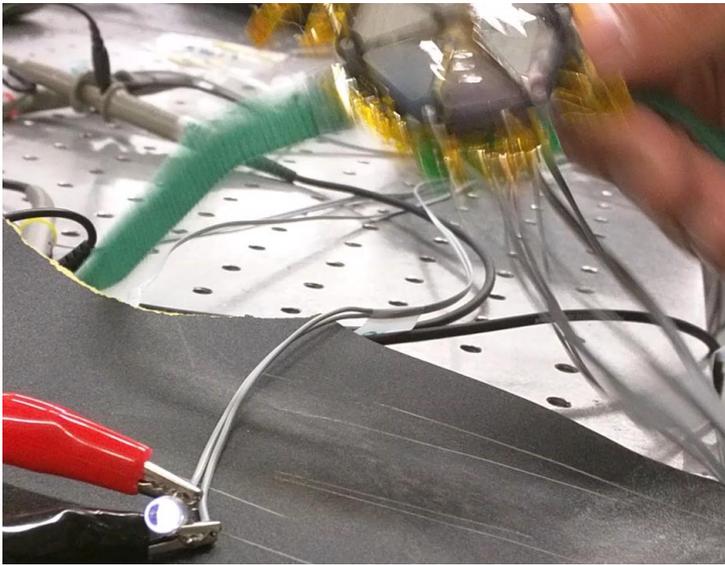


Piezo / Magnetic Harvester



Prototype and Test Results

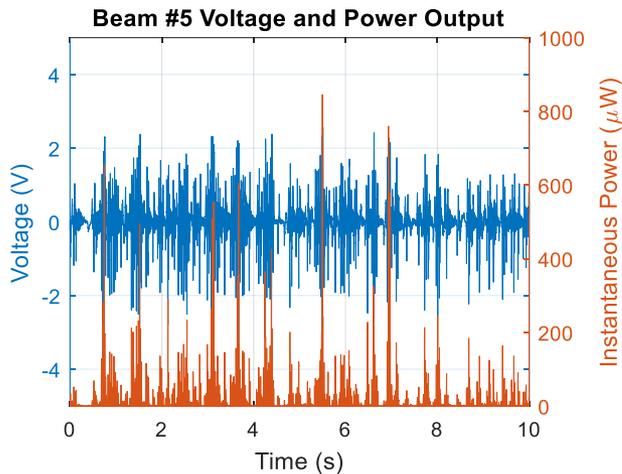
Custom fabricated thinfilm PZT



System design, and testing



Prototype and Test Results



* Best performing beam shown above, which is a single electrode (i.e. unimorph). Assumes beams perform at this equivalent level.

Input		Total Power [μW]	Total Power [μW] (best* X12)
Swing Arm $30 \sin \frac{2\pi t}{T}$	T=1s	10.3	41.8
On Wrist	Jogging in place	38.3	156.6
	Rotating the wrist	25.1	91.4
Shaking in hand	Rotor in continuous rotation	37.8	158.8

Conclusions

- There is about 1 order of magnitude gap between what current COTS (and research) devices provide ($\sim 10 \text{ uW}$) and what wearable systems need ($\sim 100 \text{ uW}$)
- Theory indicates that it is possible to close that gap in a $\sim \text{cm}^3$ size device ... but technological solutions will need to be developed that approach the theoretical maximum
- Eccentric rotor based devices are promising ... but there may be other approaches that could get closer to the theoretical maximum

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